

Recent and Ongoing Developments in LS-DYNA

Dilip Bhalsod



12th Oasys LS-DYNA Indian Update Meeting
March 2019



Announcement



As of March 04, 2019 Nathan Asher Hallquist has been appointed Executive Vice President of LSTC.

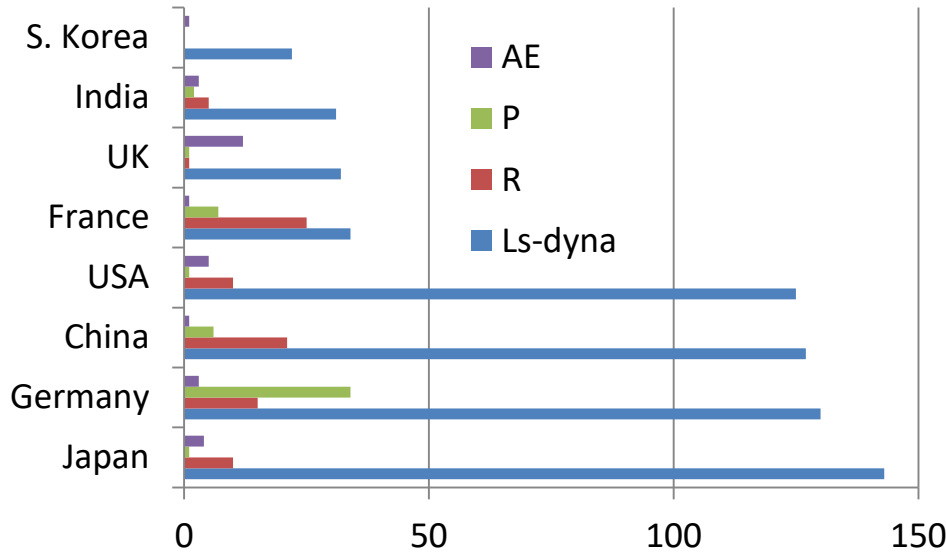
Outline

- Introduction
- Applications and development updates on
 - Metal forming
 - Implicit
 - Frequency Domain Analysis
 - Material: composite
 - CFD: ICFD, ALE, SPH & CESE
 - Meshless method
- Summary & Future

Introduction

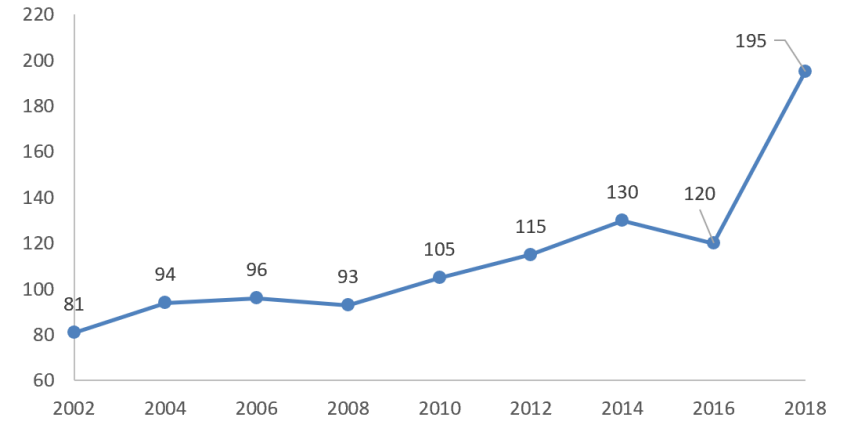
Growth of LS-DYNA

- Continues leading explicit FEA

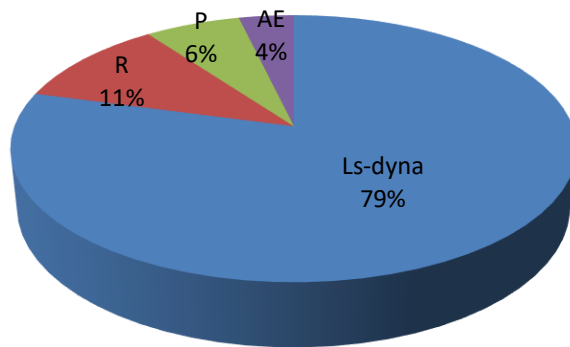


- Keeps growing

CONFERENCE PAPERS

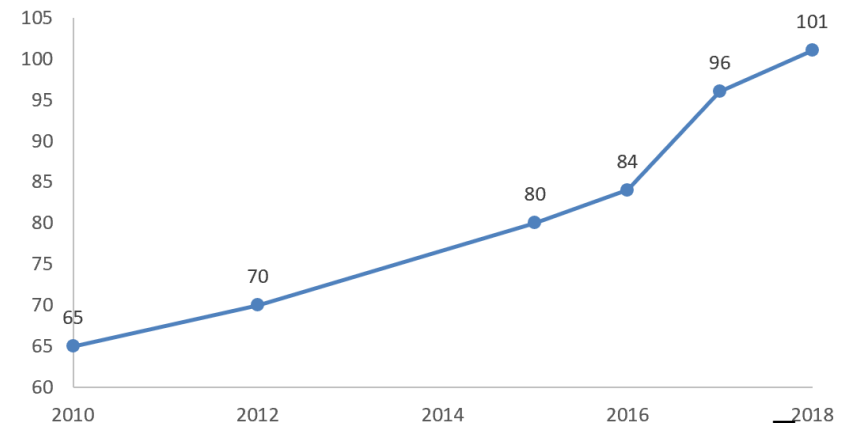


Explicit CAE openings in Indeed, 05/04/2018



Global Market Share

STAFF



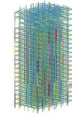
LS-DYNA Applications

Development costs are spread across many industries



Automotive

Crash and safety
NVH & Durability
FSI



Structural

Earthquake safety
Concrete and composite structures
Homeland security



Aerospace

Bird strike
Containment
Crash



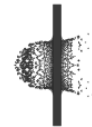
Electronics

Drop analysis
Package analysis
Thermal



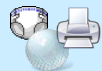
Manufacturing

Stamping
Forging
Welding



Defense

Weapons design
Blast and penetration
Underwater Shock Analysis



Consumer Products



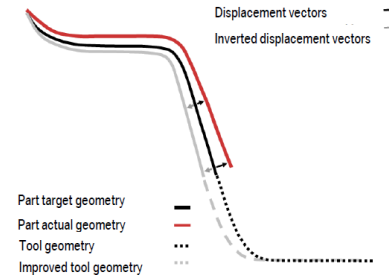
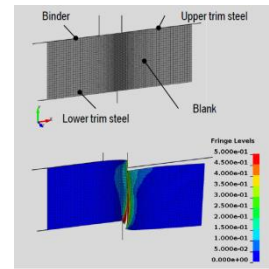
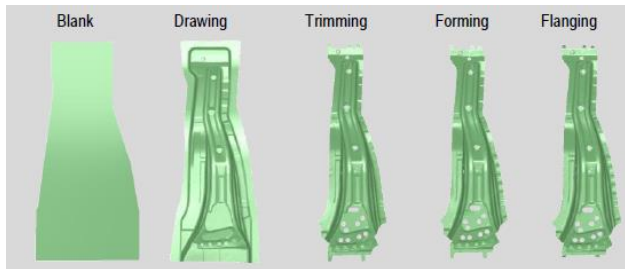
Biosciences

Forming Simulation

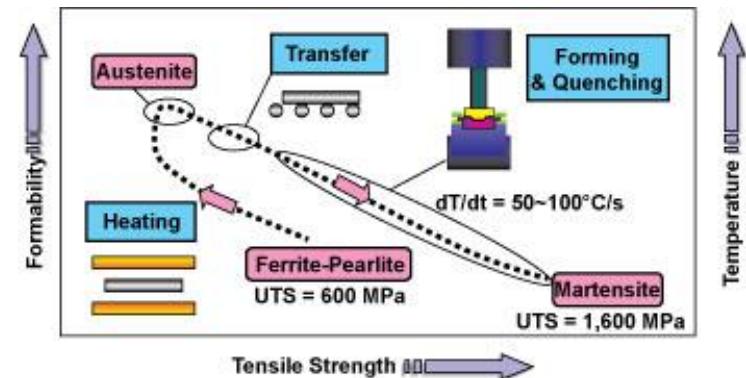
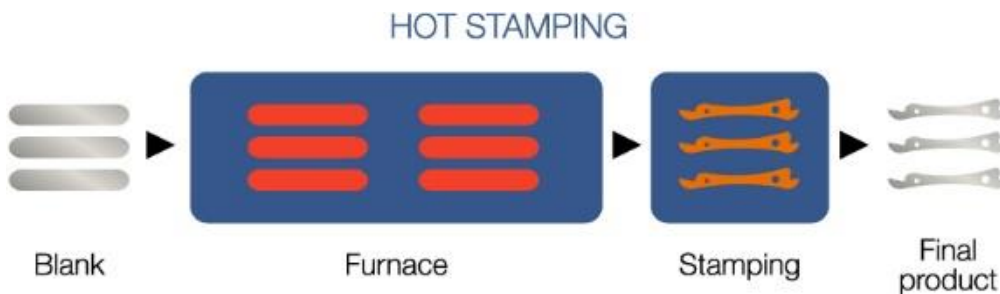
L. Zhang, X. Zhu, F. Ren

LS-DYNA for forming

- Users include, not limited to,
 - Audi, BMW, Volvo, Honda, Mazda, Nissan, Toyota, Unipres,..
- Usage of LS-DYNA for Metal Forming in BMW
 - cold forming, trimming and springback compensation



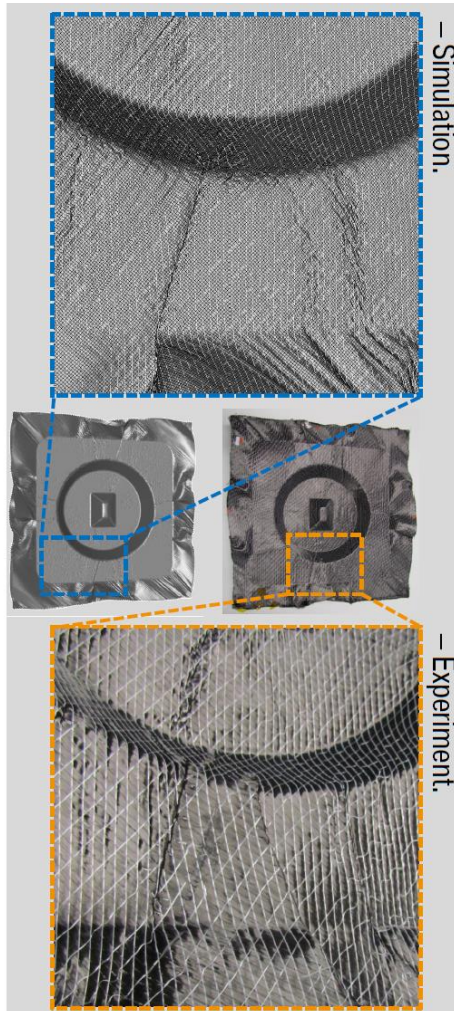
- simulation of indirect press hardening.



LS-DYNA for forming in BMW

- Draping of CFRP

LS-dyna

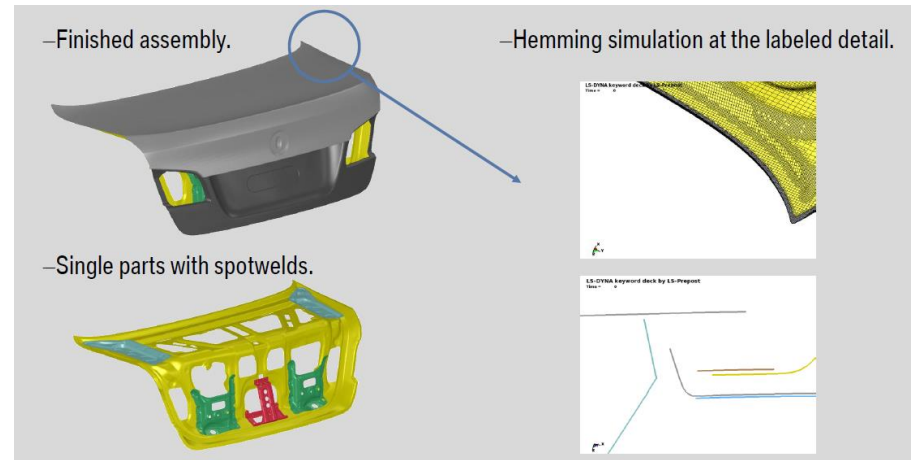


- Assembly process,



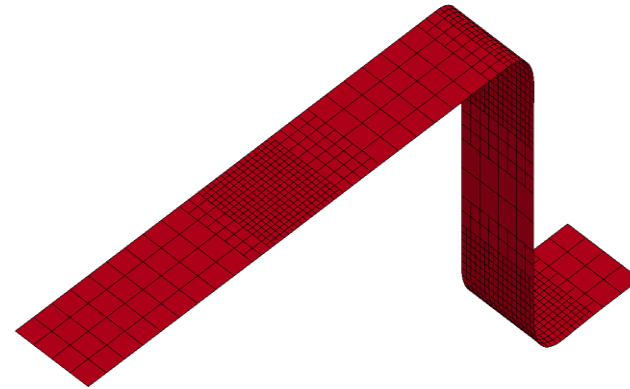
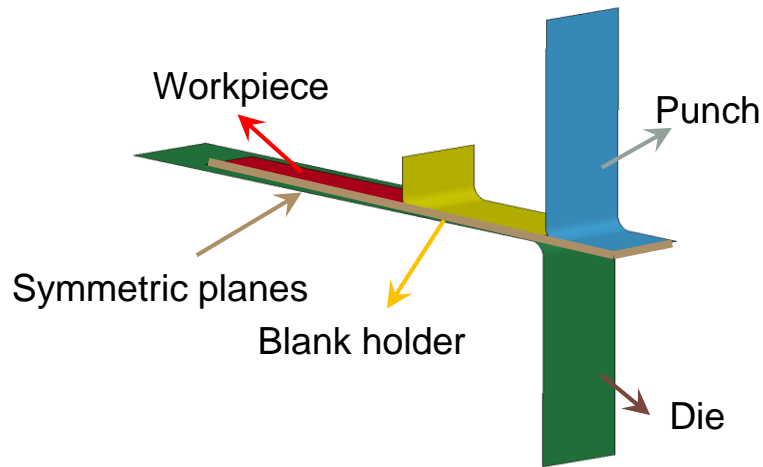
- Insertion of single parts
- Modeling of spotwelds, weldlines & adhesive
- Hemming simulation of the outer parts

Test

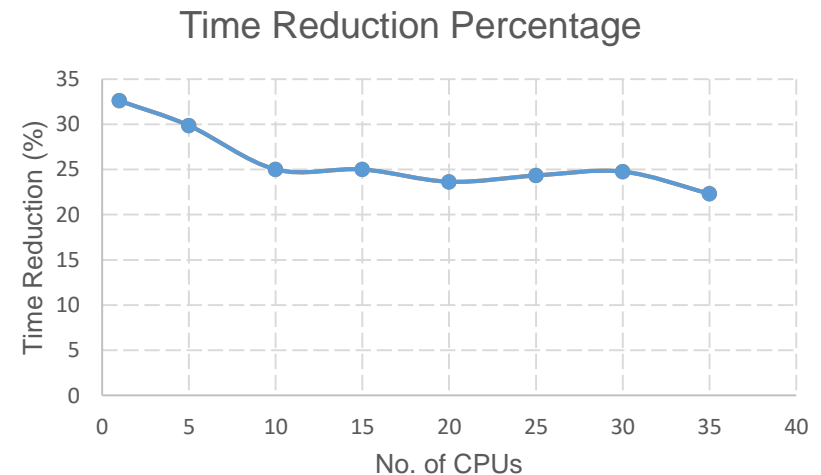


MPP Fusion

- As per BMW's request, Fusion is extended to MPP

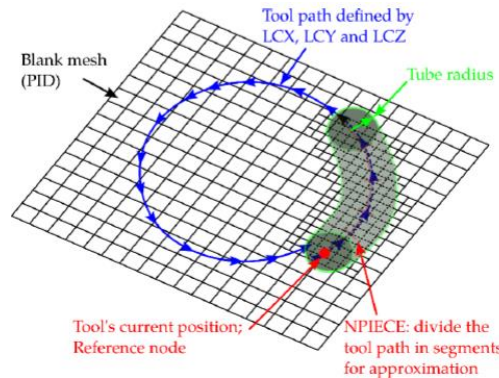
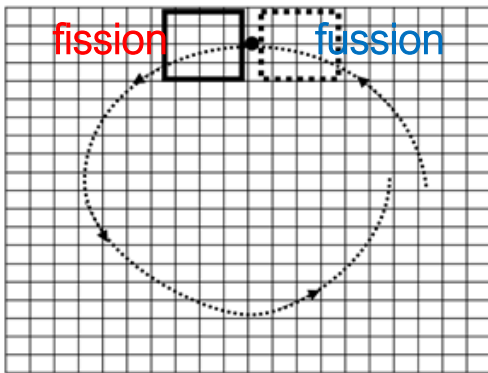


- MPP performance
 - Reduce simulation time $> 25\%$
 - Forming error $< 2\%$
 - Springback error $< 10\%$



Tube-adaptive method

- Box-adaptive method
 - Cannot handle arbitrary loading path
 - Need to perform mesh fission/fusion every single time step



LS-DYNA keyword deck by LS-PrePost

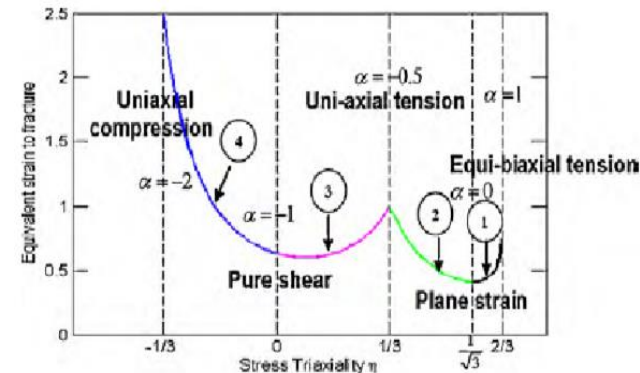
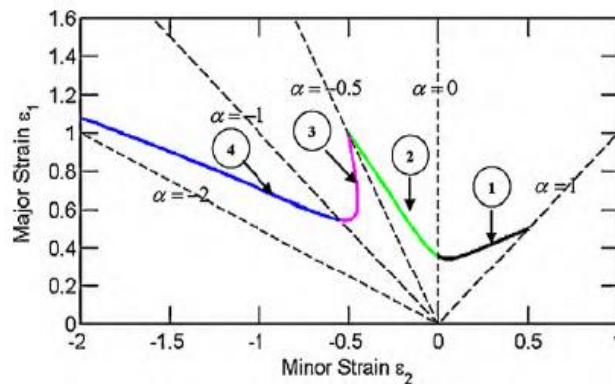


- Tube-adaptive method
 - Arbitrary loading path
 - Optimal adaptive time interval and tube radius
 - Reduce computational cost while maintaining accuracy

Radius	2	4	6	8	10	12	14	16
Thick. Diff.(%)	6.4	4.4	5.2	1.8	0.3	0.7	0.9	0.6
Time Red.(%)	50	50	49	47	46	45	44	40

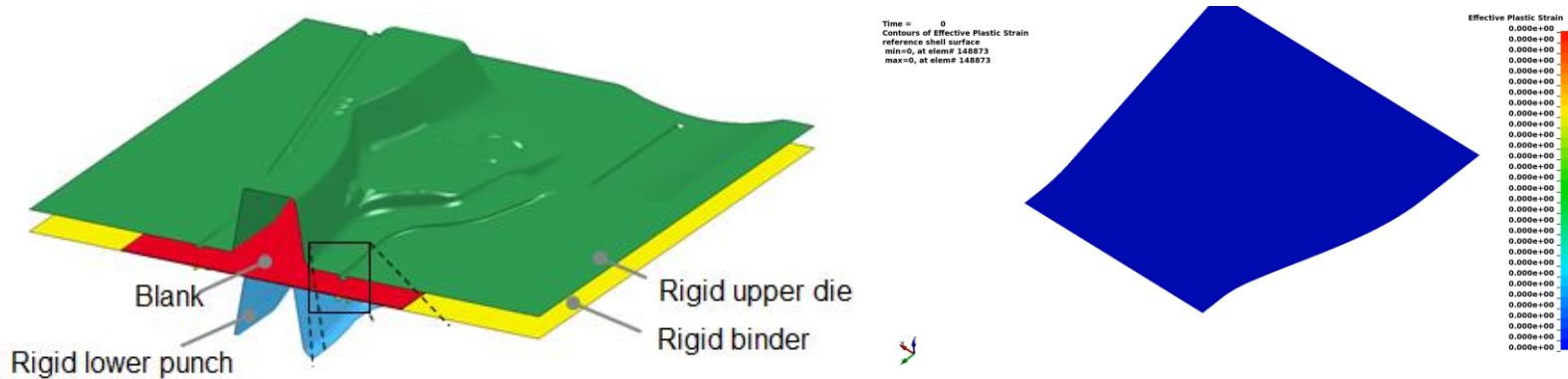
Translations between FLD and Triaxial Limit

- Increasingly, as more Advanced High Strength Steels (AHSS) are being used, stamping engineers need to worry about material failure such as shear fracture during forming, in addition to the traditional necking failure.
- Two keywords are created to conveniently translate the two types of failure limits.
 - *DEFINE_CURVE_FLD_FROM_TRIAXIAL_LIMIT
 - *DEFINE_CURVE_TRIAXIAL_LIMIT_FROM_FLD



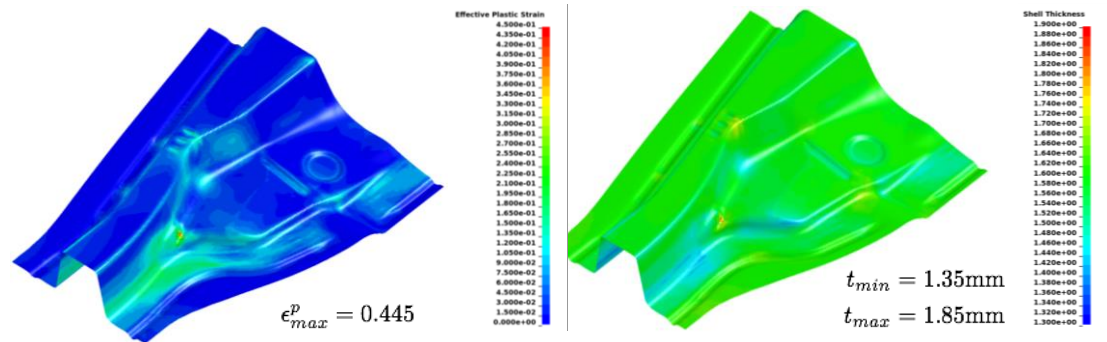
IGA for Metal Stamping

- NUMISHEET 2005 benchmark in 2017



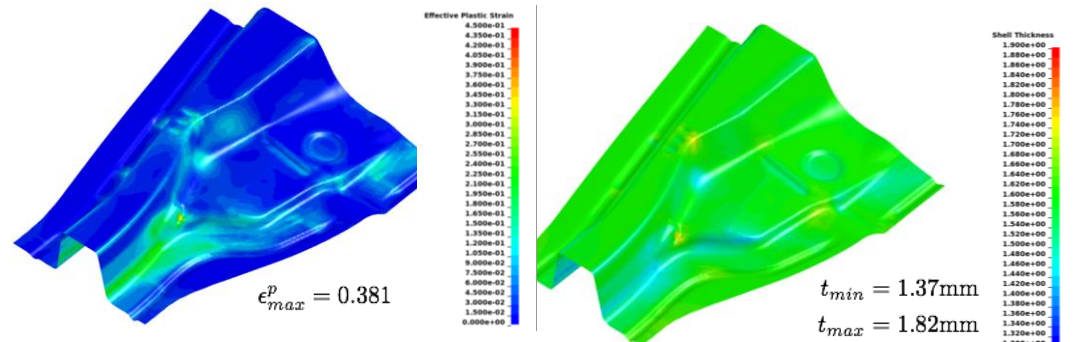
FEA:

- Avg. mesh = 2mm
- 3.7 hr



IGA:

- No adaptivity
- Mesh = 4mm
- 2.2 hr

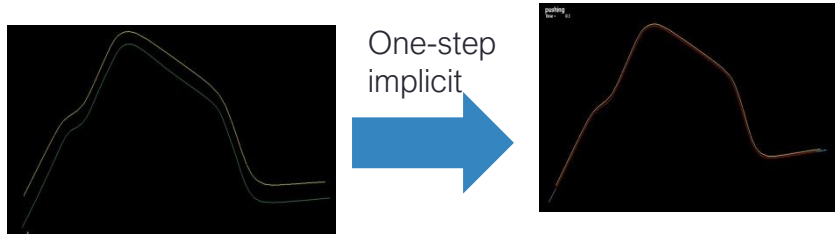


Implicit

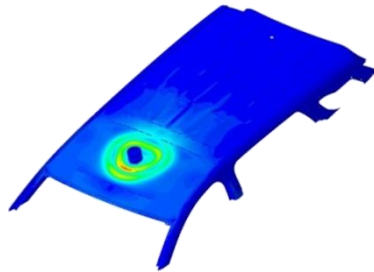
Thomas Borrvall, F. Bengzon

LS-DYNA for Implicit analysis

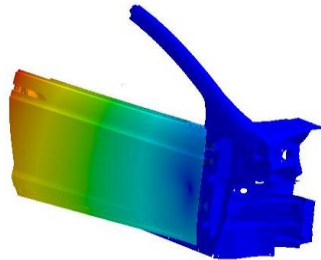
- Spring-back compensation



- Static structure analysis



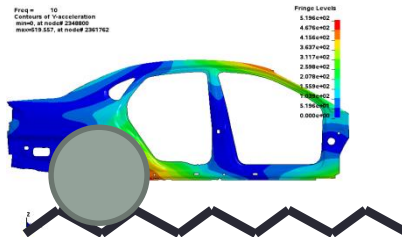
Oil canning simulation



door sag simulation

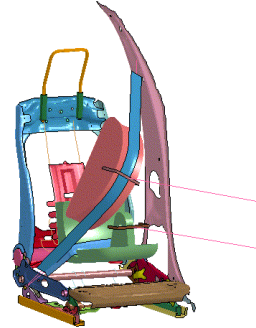
- Frequency domain solver for NVH, fatigue, random vibration analysis..

$$F(t) = F_0 \sin(\omega t + \phi)$$



- Safety analysis

LS-DYNA keyword deck by LS-PrePost
Time = 0



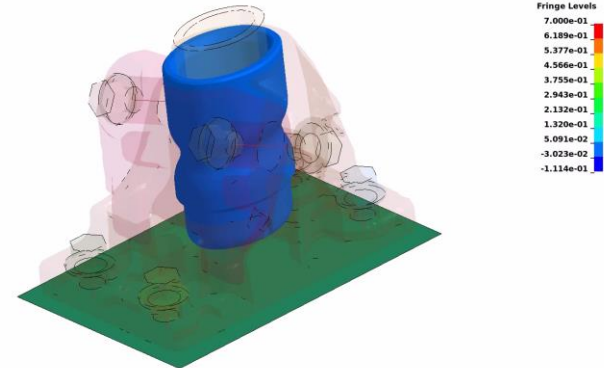
207/210



Positioning BioRid & HPM, Daimler

- Other

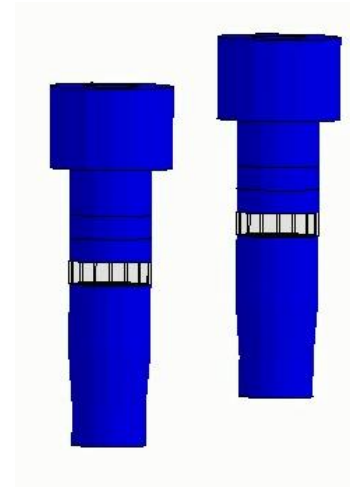
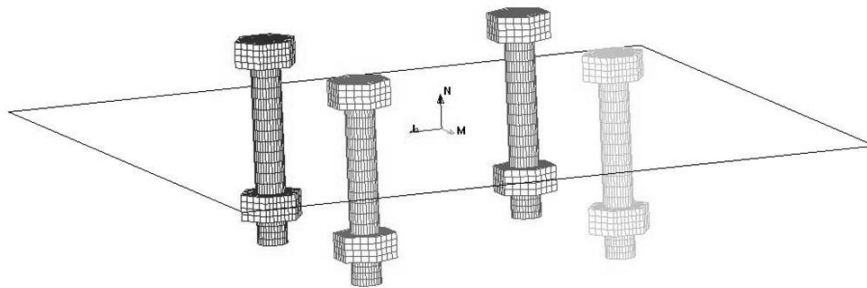
Time = 0
Contours of Pressure
reference shell surface
min=-1.46802e-16, at elem# 7029847
max=1.17269e-16, at elem# 7020664



Fitting of rubber cylinder between two steel components, VOLVO GTT

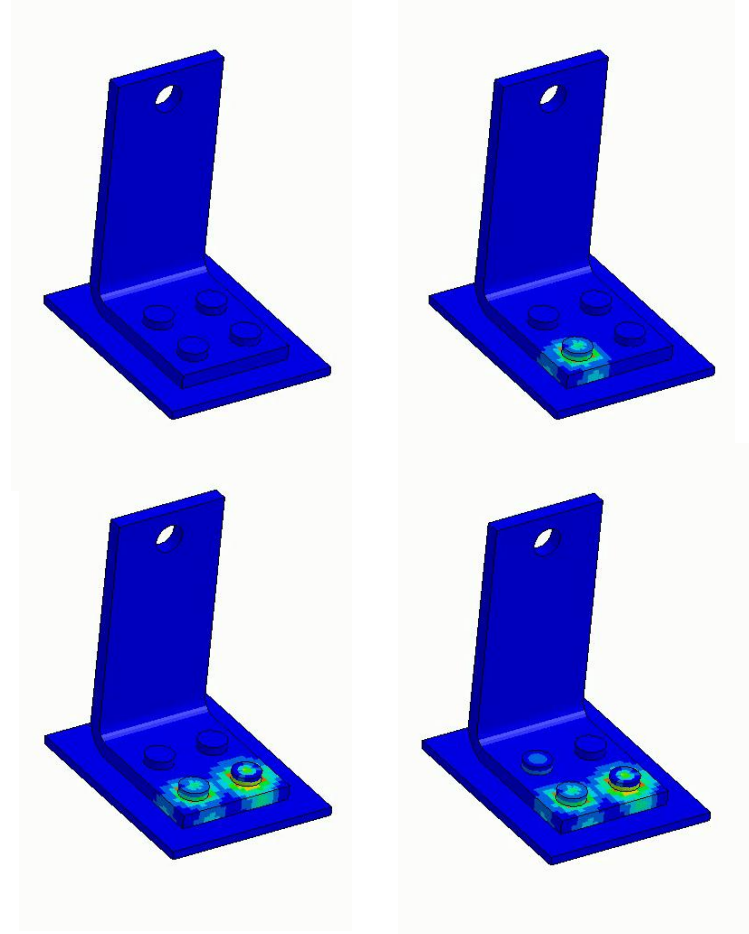
Improvement for implicit

- Prescribed motion
 - exact integration of velocity and acceleration curves
 - avoid zero residual force for use on rigid bodies
- Mortar contact
 - frictional torque due to (shell) offsets
 - extensions of friction, tiebreak and tied weld
 - Rejections
- Prestress
 - initial stress section accounts for bending
 - IZSHEAR=2 on *INITIAL_STRESS_SECTION
 - mean cross sectional stress prescribed
 - preserves structural integrity of bolts



Improvement for implicit

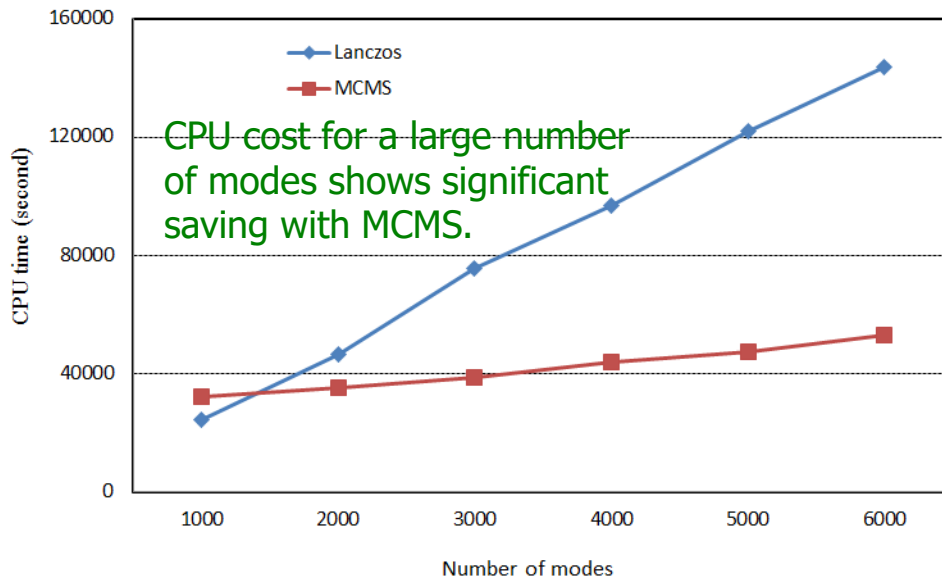
- Process splitting (*CASE)
 - implicitly requested by users
 - a "complicated" process is divided into "simple" steps
 - no birth/death, simple curves etc.
 - system state transferred between cases through dynain.lsd
 - stress, history, stabilization, contact friction, tied contact
 - flexible
 - each case is essentially a keyword input, allows for "any" modifications
 - "restart" can be made from any case
 - saves the agony of rerunning the entire process



Frequency Domain Analysis

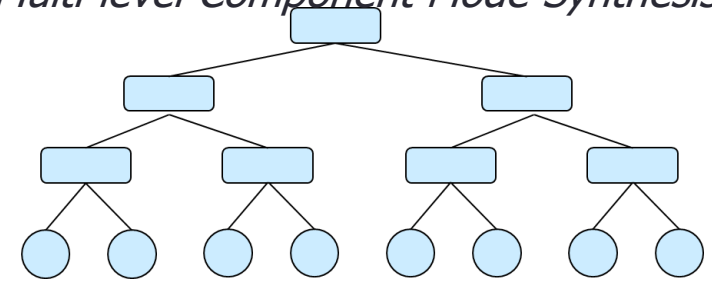
Z. Cui & Y. Huang

Using MCMS for NVH analysis



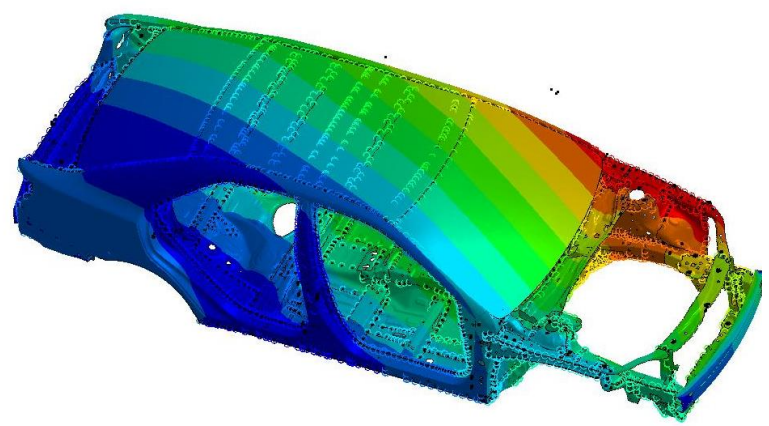
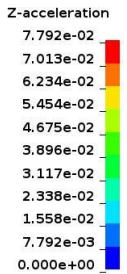
MCMS (developed by Roger Grimes)

Multi-level Component Mode Synthesis

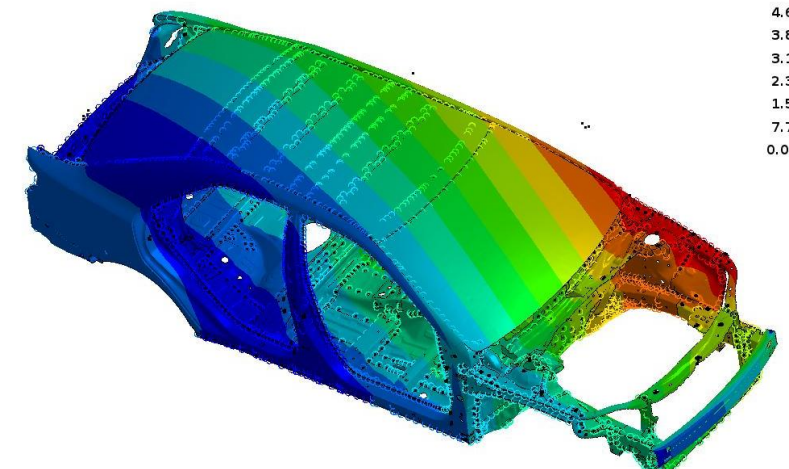


Freq = 1
Contours of Z-acceleration
min=0, at node# 384932
max=0.078038, at node# 243935

Contours of Z-acceleration
min=0, at node# 723043
max=0.0779201, at node# 244053

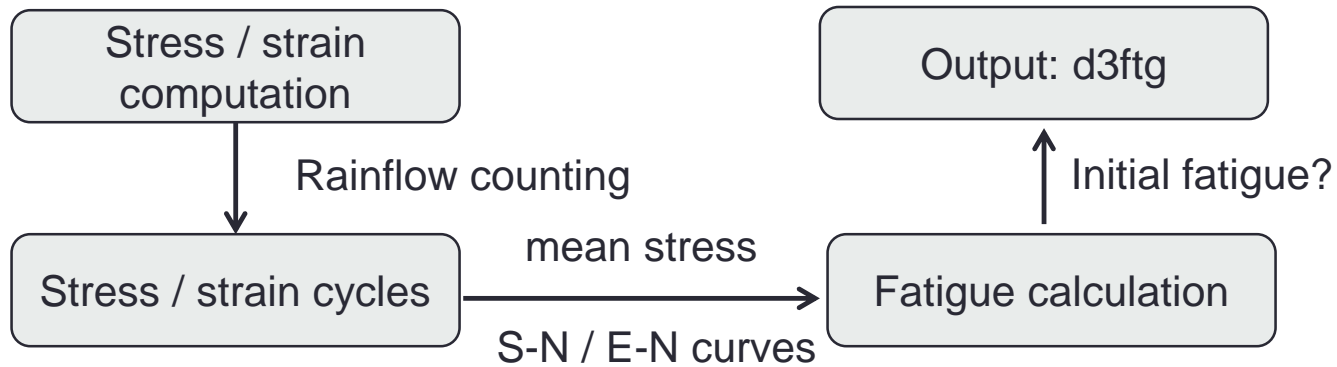


SSD results by Lanczos



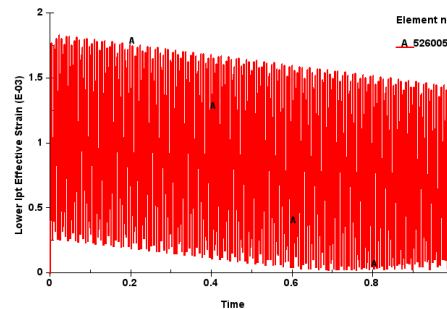
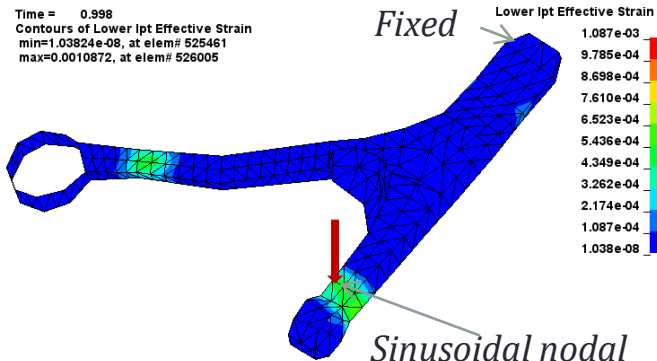
SSD results by MCMS

Time domain fatigue analysis

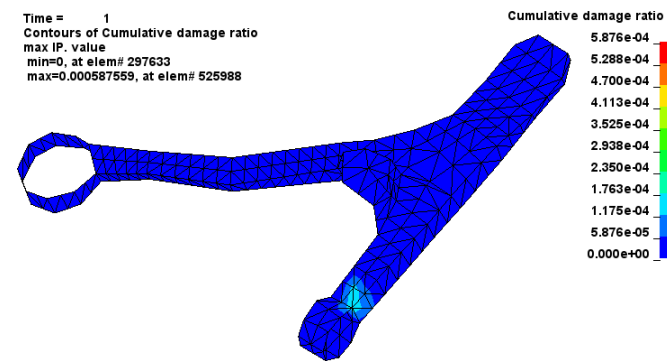


- Calculate damage ratio and fatigue life in time domain
- Advantages
 - A wide selection of stress / strain solvers (linear / nonlinear, thermal, multi-physics, fluid-structure interaction, EM, CFD, explicit / implicit, etc.)
 - Integration of vibration and fatigue solvers in one code.

Time = 0.998
Contours of Lower Ipt Effective Strain
min=1.03824e-08, at elem# 525461
max=0.0010872, at elem# 526005



Time = 1
Contours of Cumulative damage ratio
max IP. value
min=0, at elem# 297633
max=0.000587559, at elem# 525988



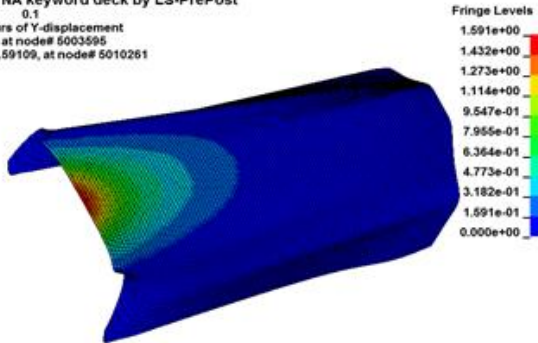
IGA for Frequency domain SSD

NURBS Shell Model

Full Gauss integration rule

Piecewise linear plasticity (*MAT_024)

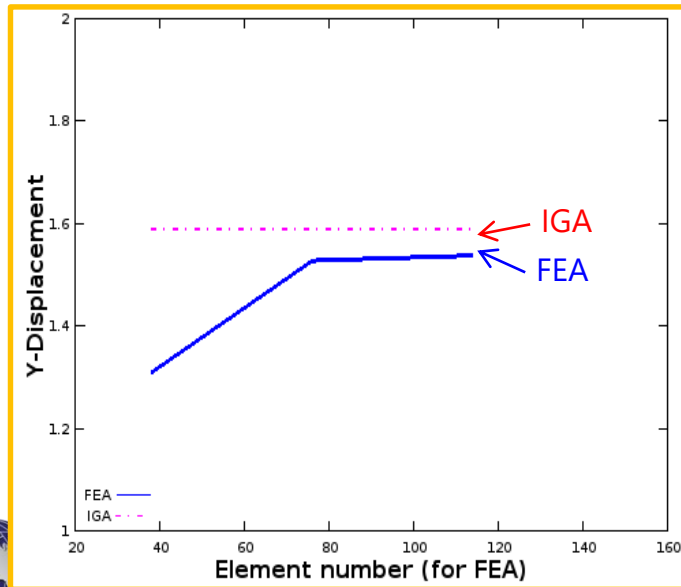
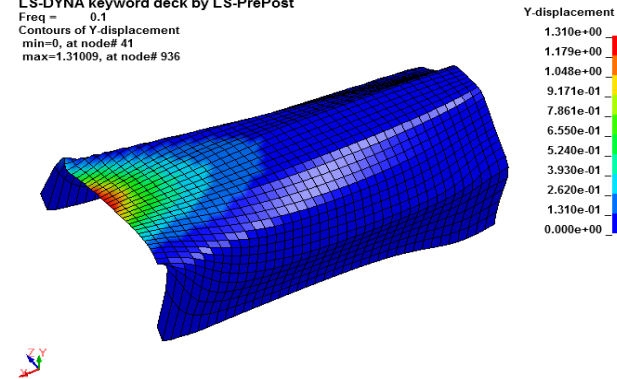
LS-DYNA keyword deck by LS-PrePost
 Freq = 0.1
 Contours of Y-displacement
 min=0, at node# 5003595
 max=1.59109, at node# 5010261



FEA baseline model

Fully integrated shell with assumed strain formulation

LS-DYNA keyword deck by LS-PrePost
 Freq = 0.1
 Contours of Y-displacement
 min=0, at node# 41
 max=1.31009, at node# 936

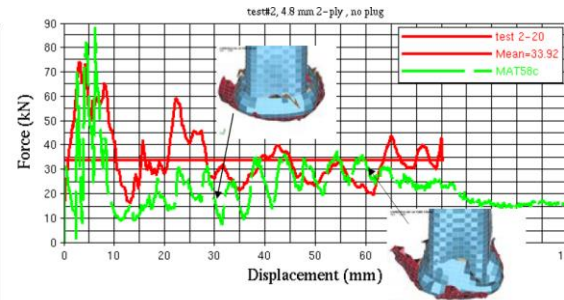
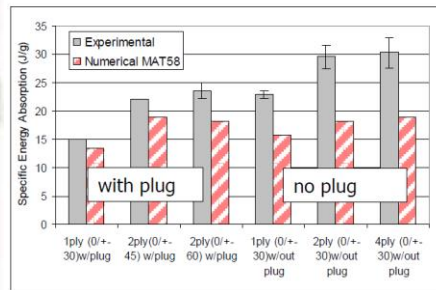


Analysis tool	Number of elements	CPU (s)
IGA	1444	47
FEA	1444	6
FEA	5776	23
FEA	12996	54

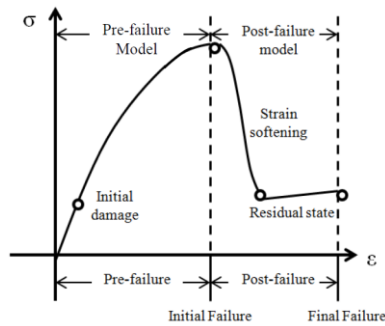
Material Composite

LS-DYNA composite material - application

- Traditional material model like MAT58 with CDM tends to underestimate the energy absorption (EA) by 10%~40%



- enhanced continuum damage mechanics (ECDM) model and a shell-beam (SB) method are developed as a remedy

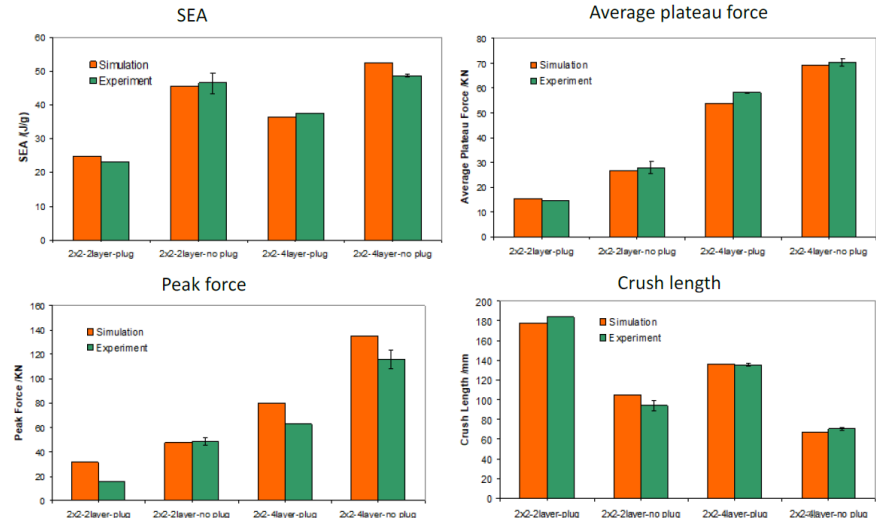


ECDM



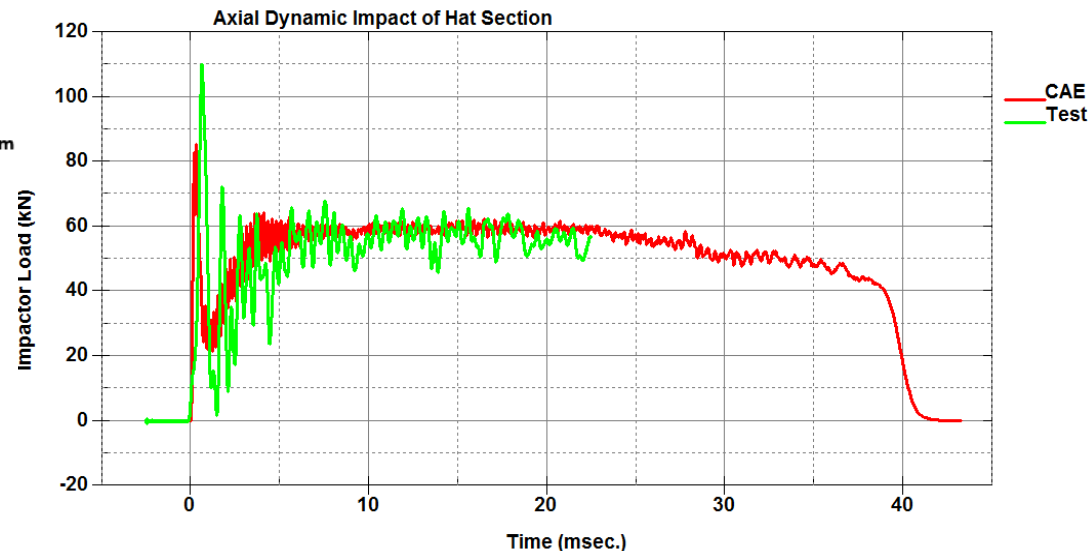
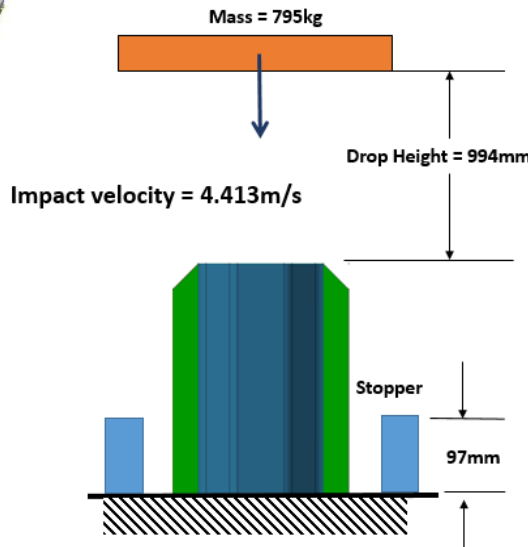
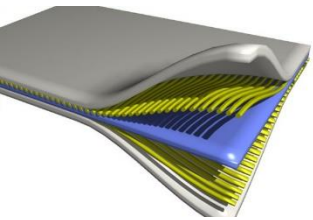
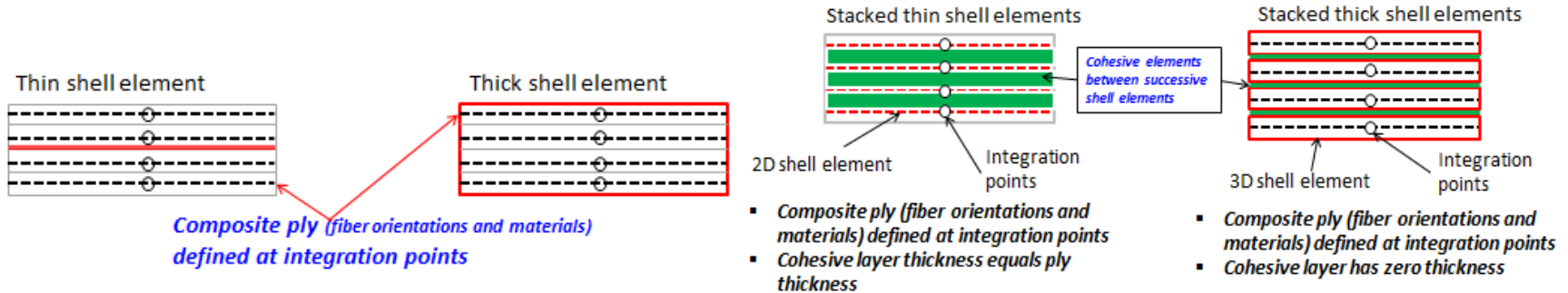
MAT58

ECDM + Shell-beam



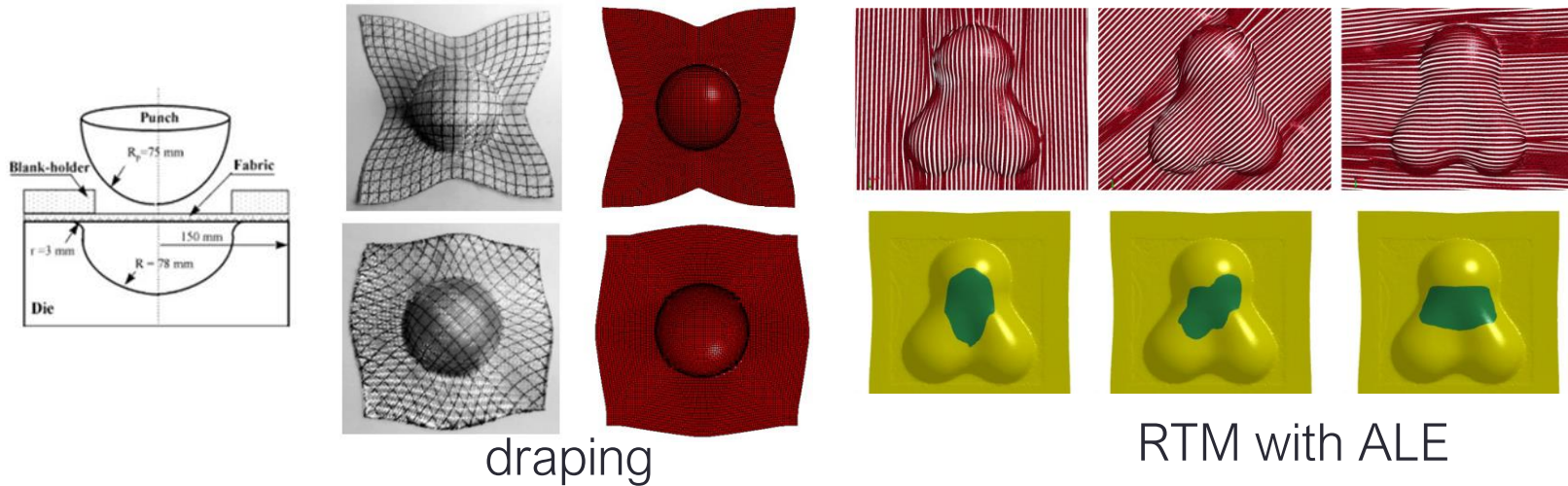
LS-DYNA composite material - application

- Pre-preg compression molded (PCM) CF composites is modeled in meso-scale using MAT_54

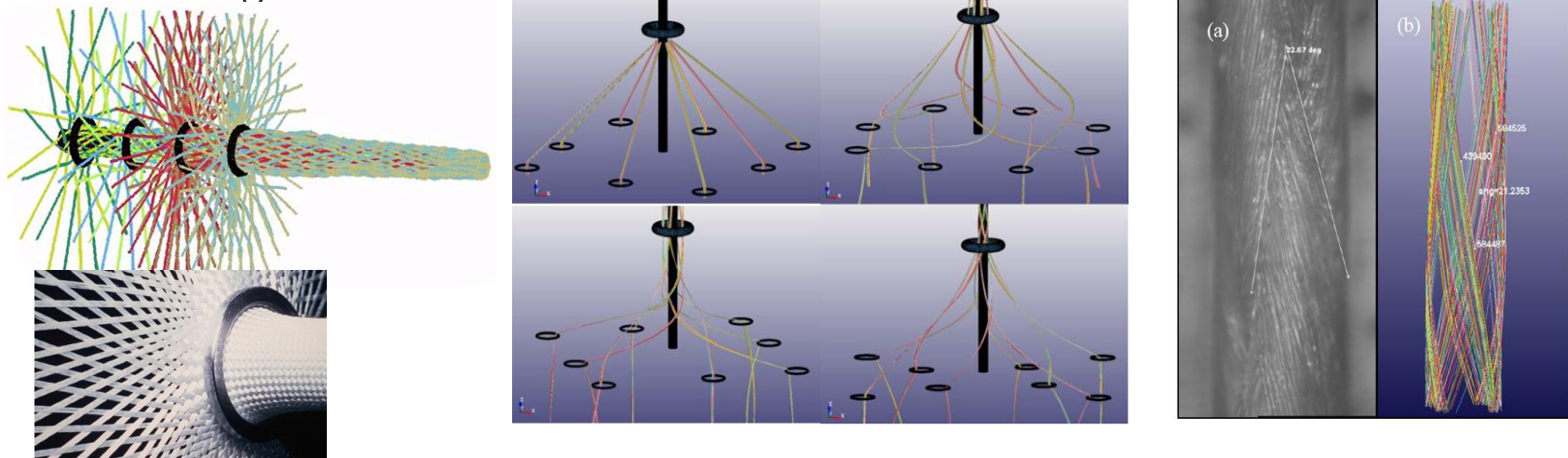


LS-DYNA composite material - application

- Draping and RTM

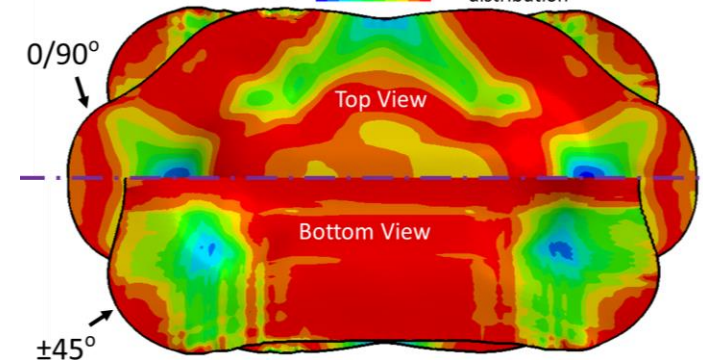
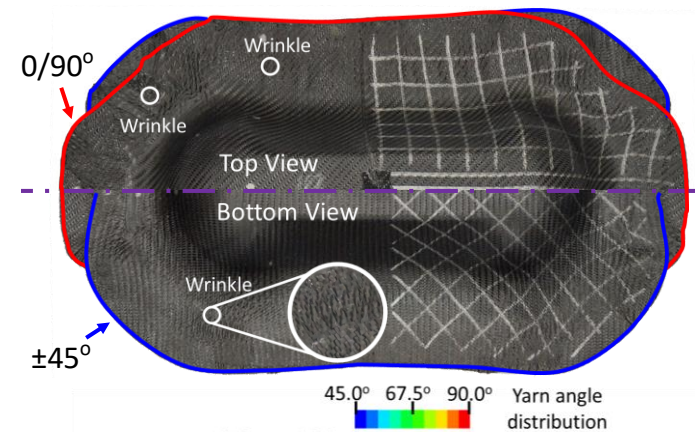
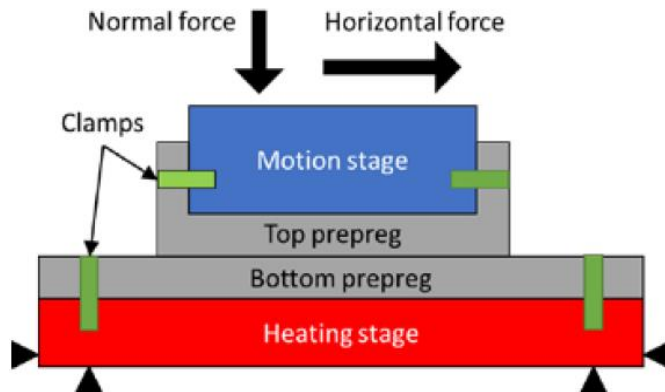


- braiding



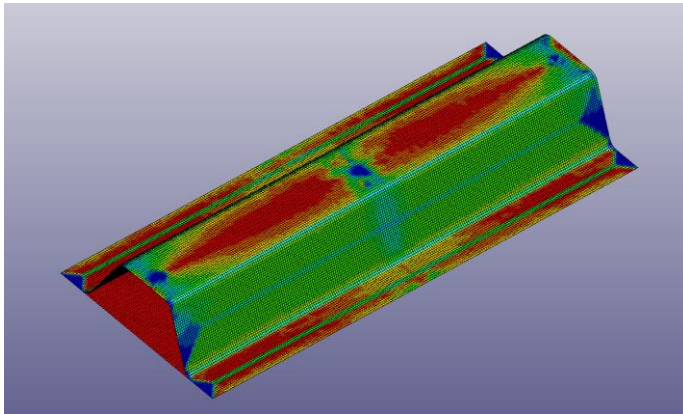
MAT_293 for the preforming of woven composites

- For woven prepregs forming simulation, which are woven CFRPs impregnated with uncured thermoset resin in desired fiber orientations
- decouple the strong tension and weak shear behavior of the woven composite under large shear deformation
- For woven long fiber composite, fiber angle after forming is critical for accurate predication of crash performance

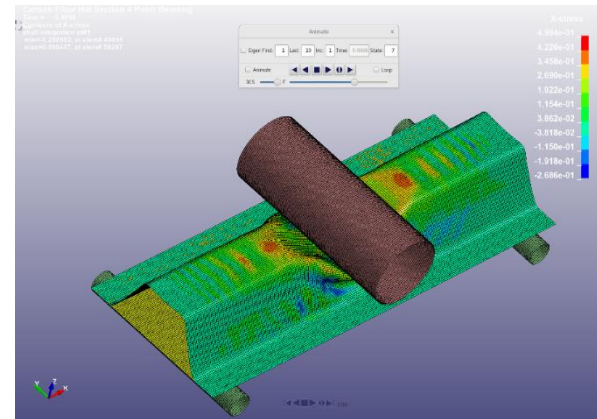


Short fiber from molding to crash

- New interface program to utilize Moldflow and MoldEx3D molding result for LS-DYNA crash analysis is recently implemented in LS-PrePost
- Enhance MAT_157 with *INITIAL_STRESS card for elasticity tensor C_{ij}



Fiber orientation result from Moldflow



LS-DYNA 3 point bending simulation

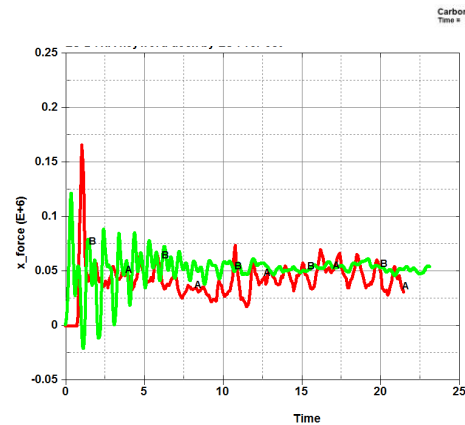
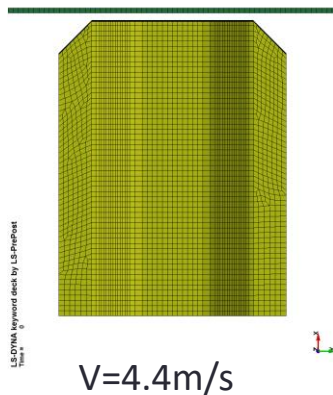
Thick shell and cohesive element for delamination

- Model description

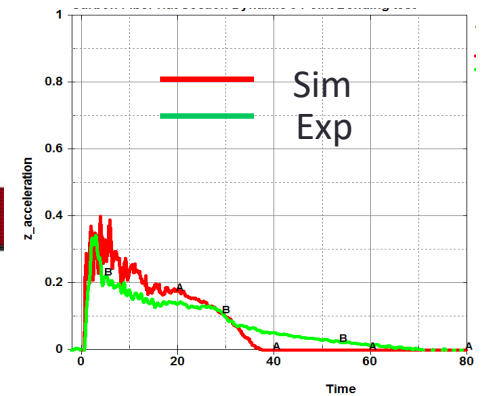
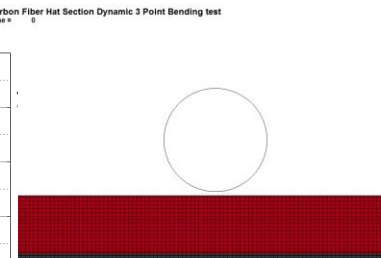
- CFRP modeled as thick shell; each thick shell represents a ply
- Cohesive element thickness of 0.01 mm; TS size 4mmx4mm
- Both UD and Woven tested
- MAT_054 is used



3 point bending



axial



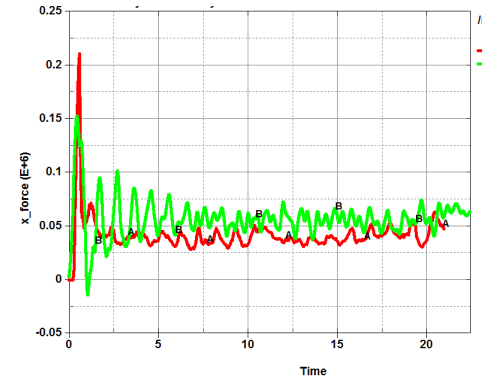
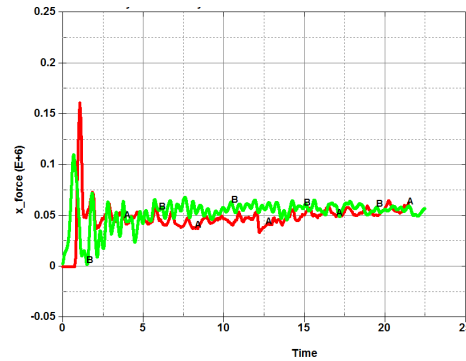
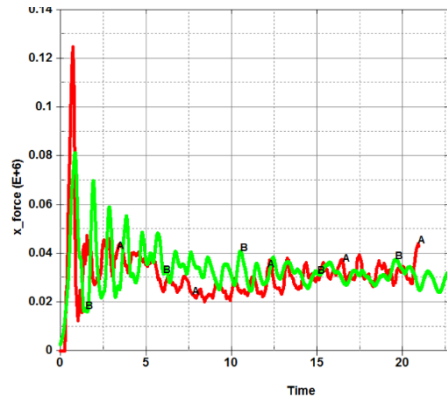
3-point bending

Woven 0-90

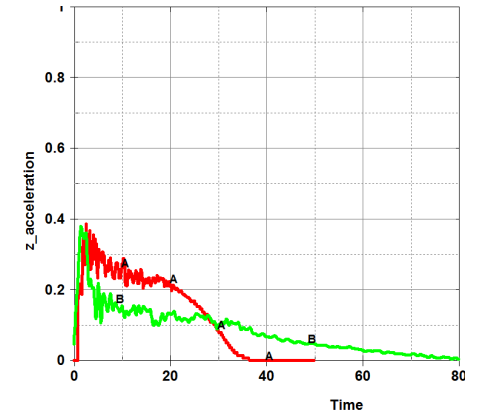
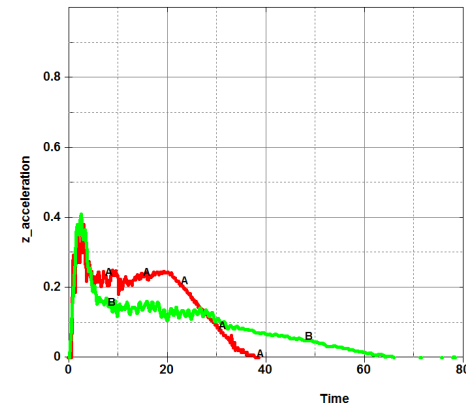
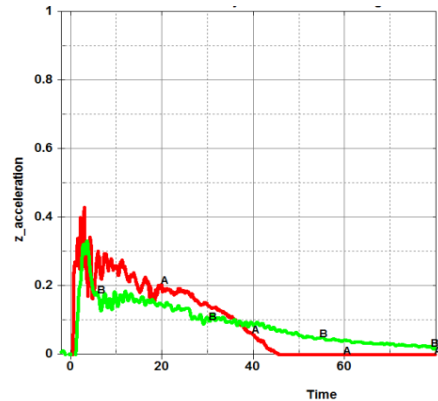
Thick shell and cohesive element for delamination

— Sim
— Exp

Axial crush



3 point bending



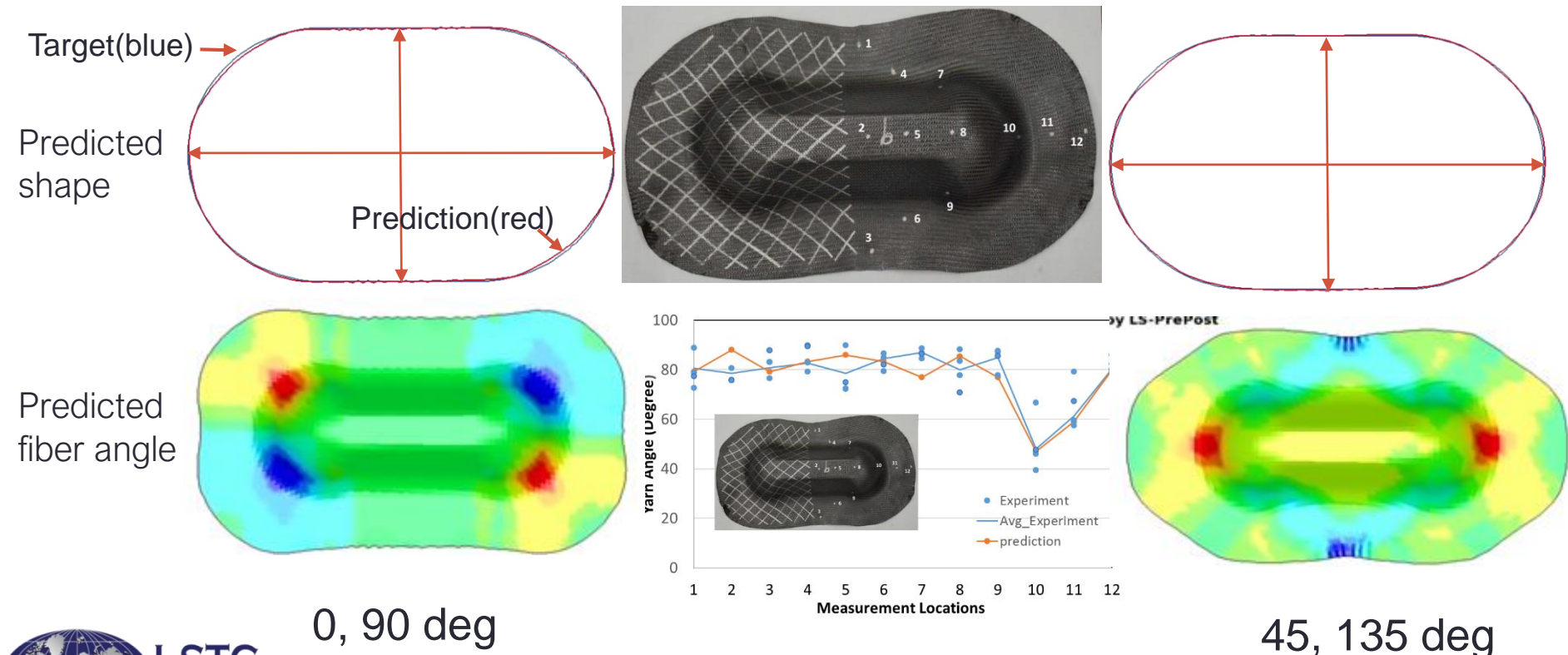
Woven
45-45

UD
[0/60/-60/0/60/-60]_s

UD
[0/90/90/0/0/0]_s

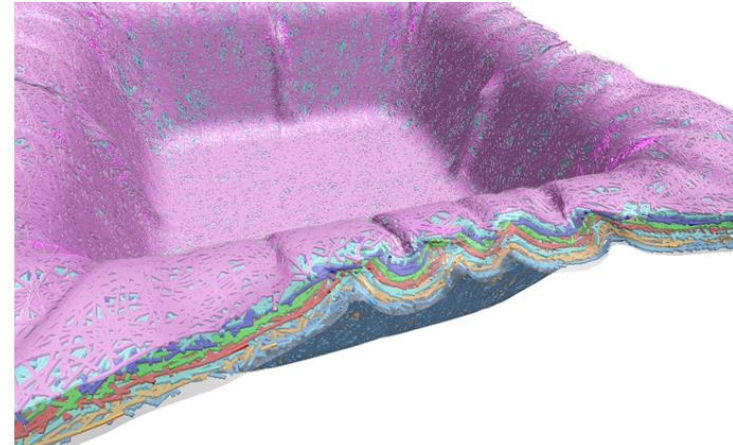
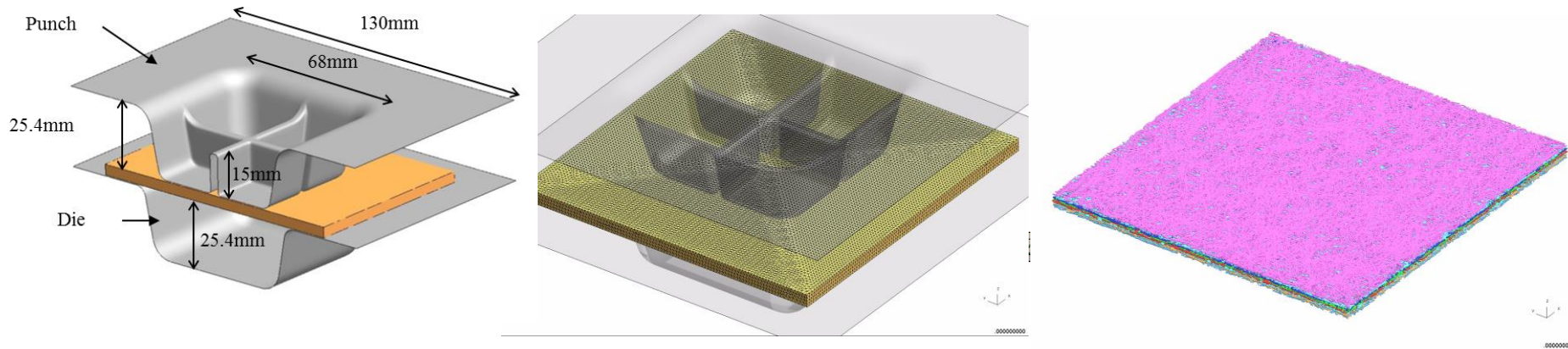
One-Step Analysis for Woven Carbon Fiber Composite

- *DEFINE_FIBER
 - defines carbon fibers and their related properties in a matrix for a one-step inverse forming simulation.
 - Can predict the desired composite shape and fiber orientations
 - works *only* with the keyword *CONTROL_FORMING_ONESTEP



*CONSTRAINED_BEAM_IN_SOLID

- Was designed for RC; Extended to simulate FRP manufacturing process
- Thermal-mechanical Adaptive EFG method with local refinement



CFD Technique

Zeng-chan Zhang, Kyoung-Su Im, and Grant Cook, Jr.

Hao Chen

Inaki Caldichoury, Pieree L'Eplattenier

Edouard Yreux

CFD solvers in LS-DYNA

- Available CFD solvers in Is-dyna

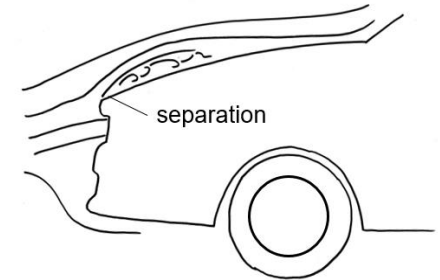
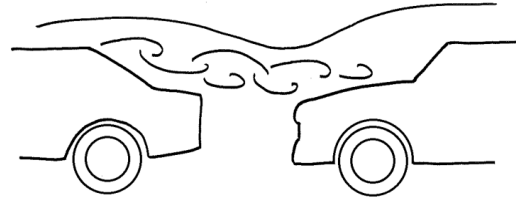
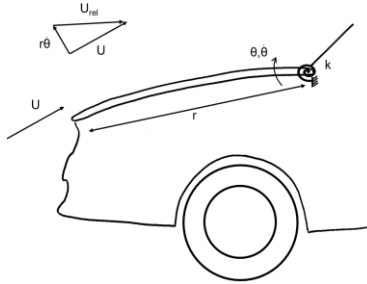
Solver	CESE	ICFD	ALE	SPH
Low speed aerodynamics	-	√	-	-
High speed aerodynamics	√	-	-	-
Explosive with EOS	-	-	√	√
Airbag-piston	√	-	√	-
Free surface problem (slamming)	-	√	√	√
FSI	√	√	√	√
Chemistry reaction	√	-	-	-
Stochastic particles	√	-	-	-

ICFD

Facundo Del Pin
Iñaki Çaldichoury
Rodrigo R. Paz
Chien-Jung Huang

ICFD applications

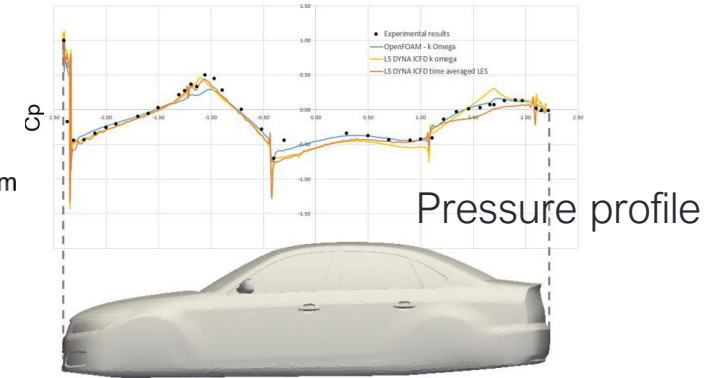
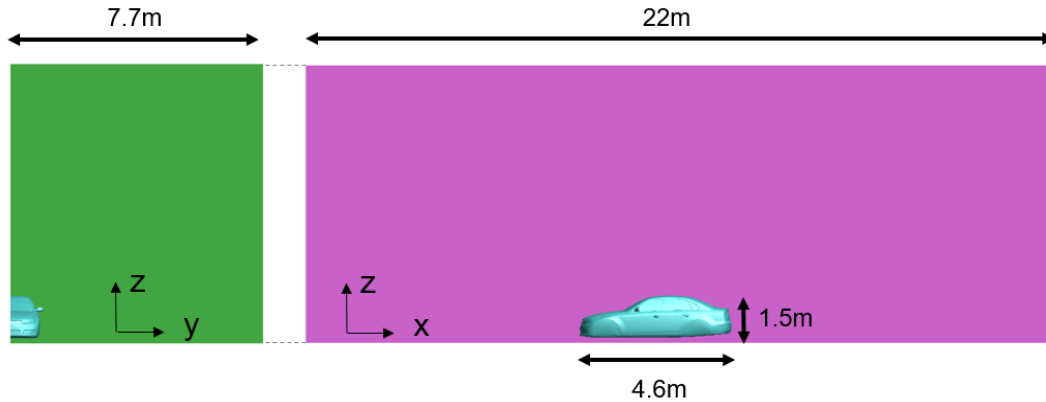
– Hood flutter vibration



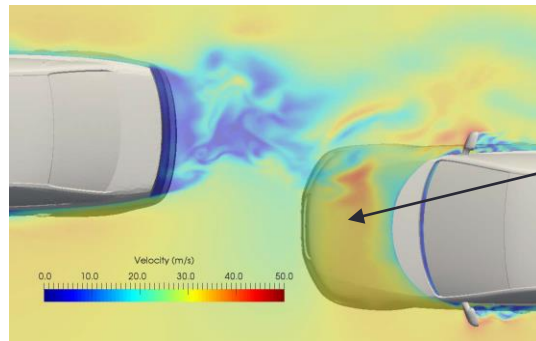
Hood attached to a rotational spring

Extraneously induced excitation

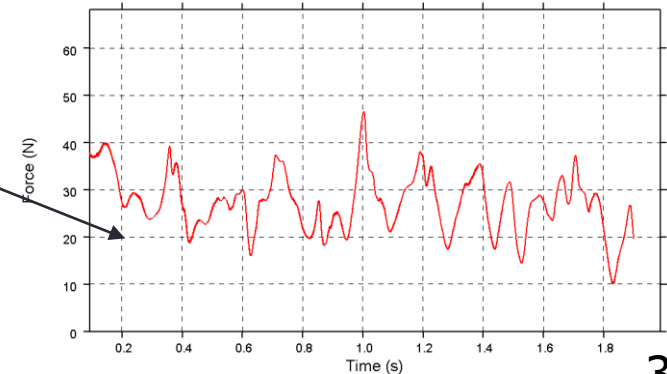
“Instability induced excitation”



Flow field around the front of the following car

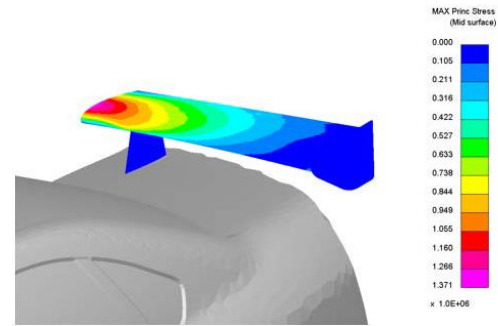
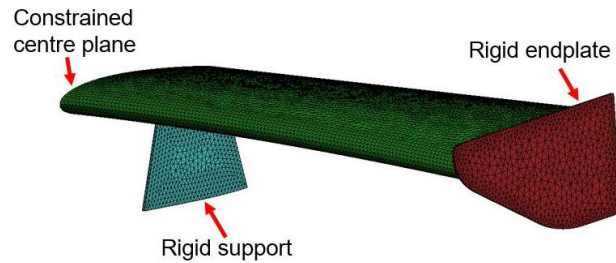


Force on the hood of the following car

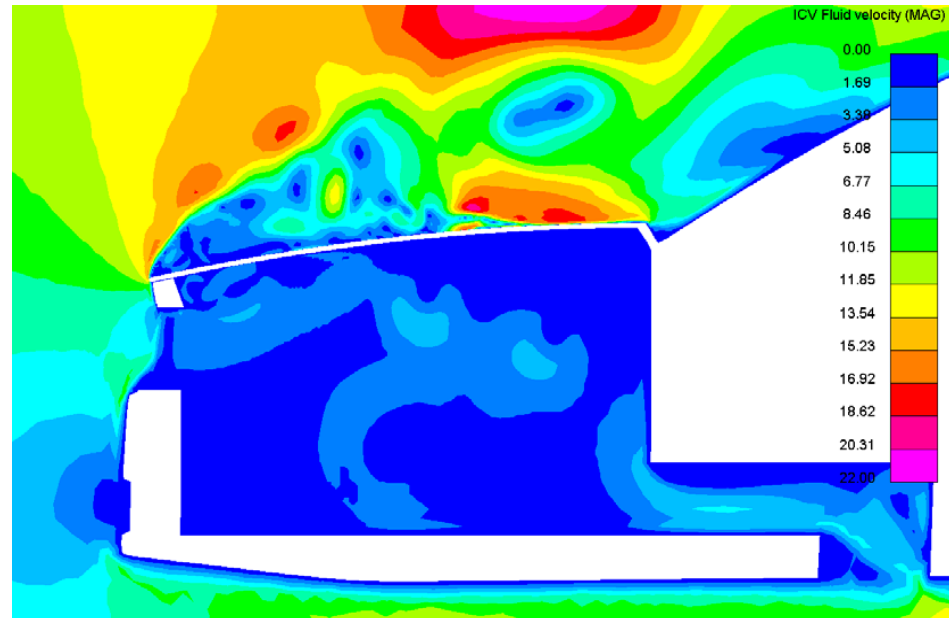
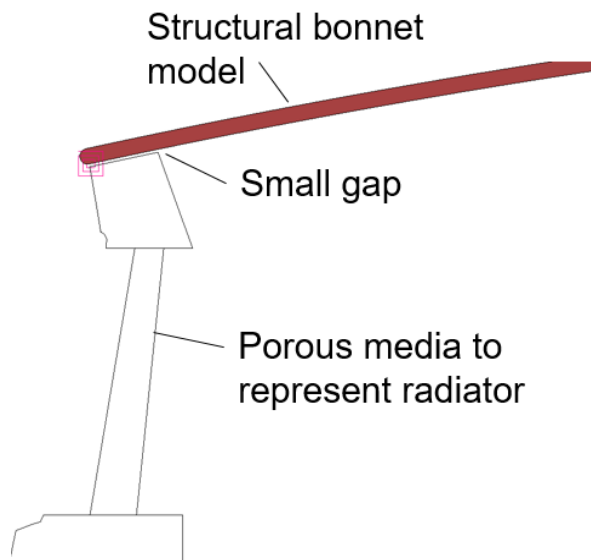


ICFD applications

- Stress on a deformable spoiler

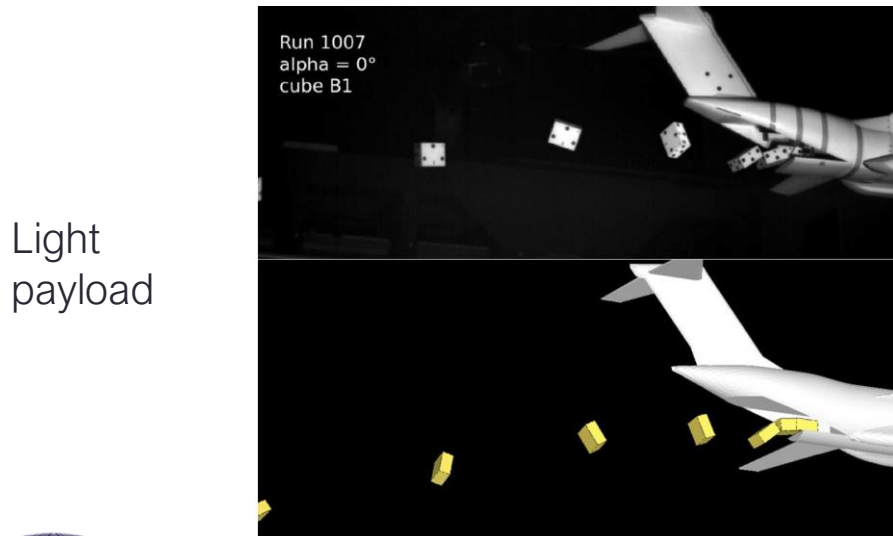
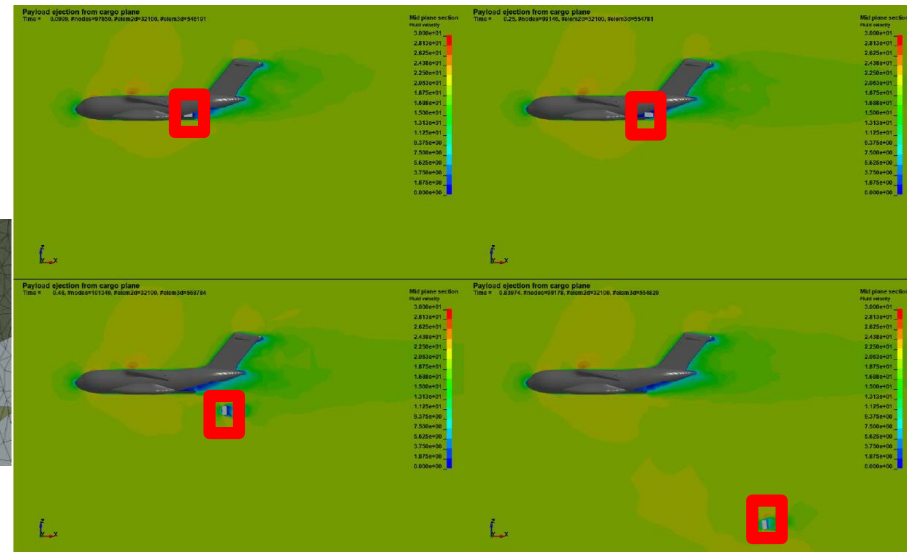
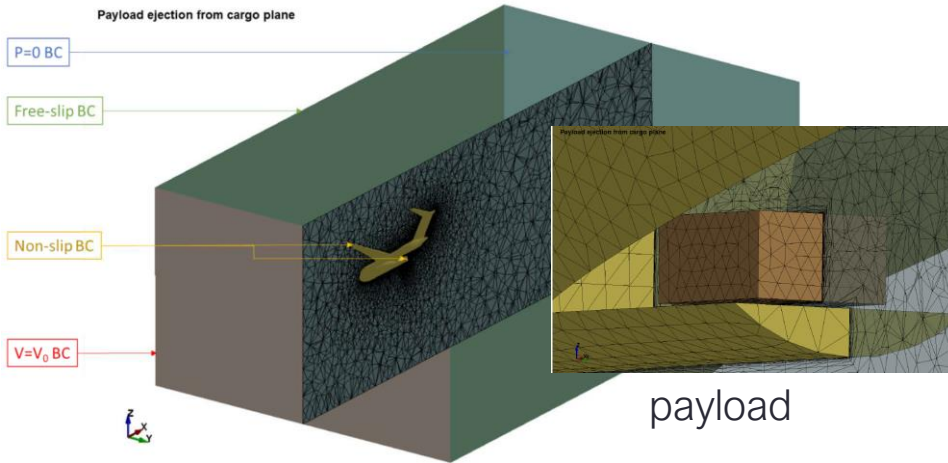


- 2D simulation of a deformable hood



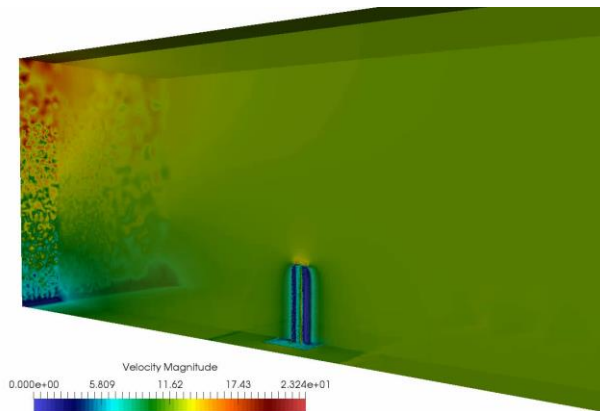
ICFD applications

- Airdrop simulation

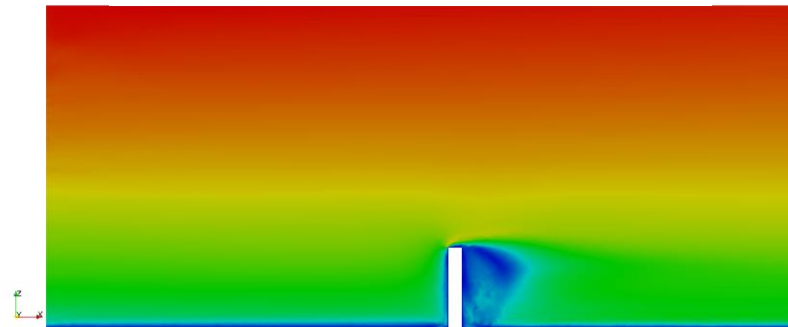
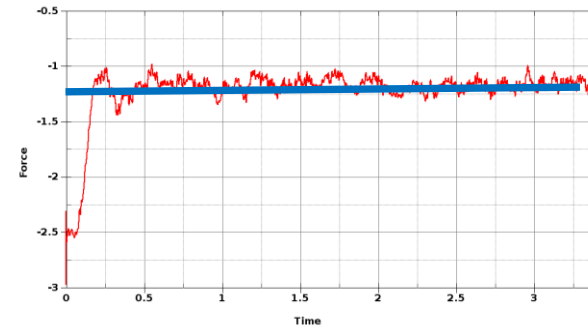


Steady State for Conjugate Heat and FSI

The steady state solver or the potential flow solver allow for a fast linearization of Fluid Structure Interaction (FSI) and/or Conjugate Heat transfer (CH) problems



Steady state analysis allows engineers to study physical problems in a time average fashion.



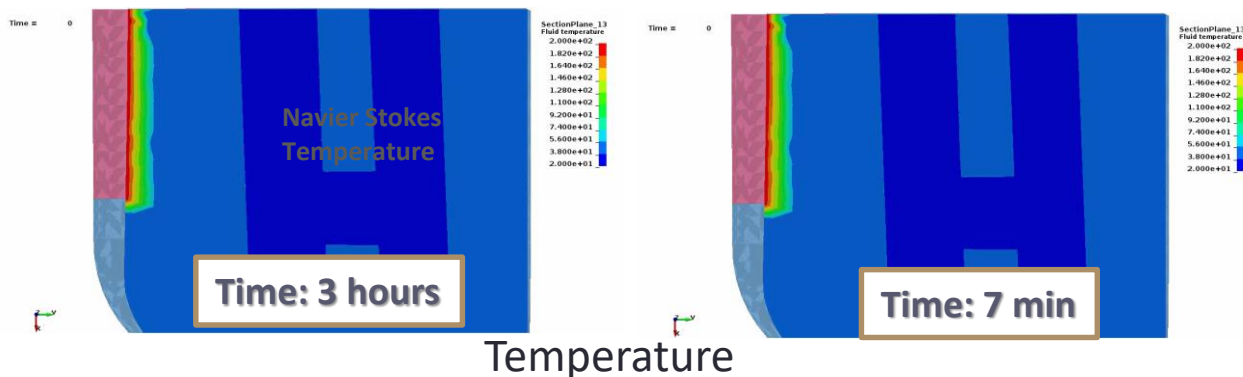
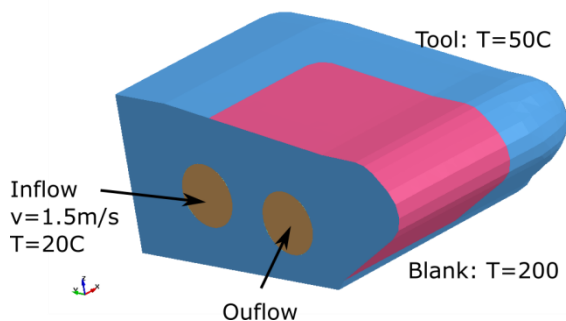
These simulation provide valuable insight faster useful for prototyping.

Steady State for Conjugate Heat and FSI

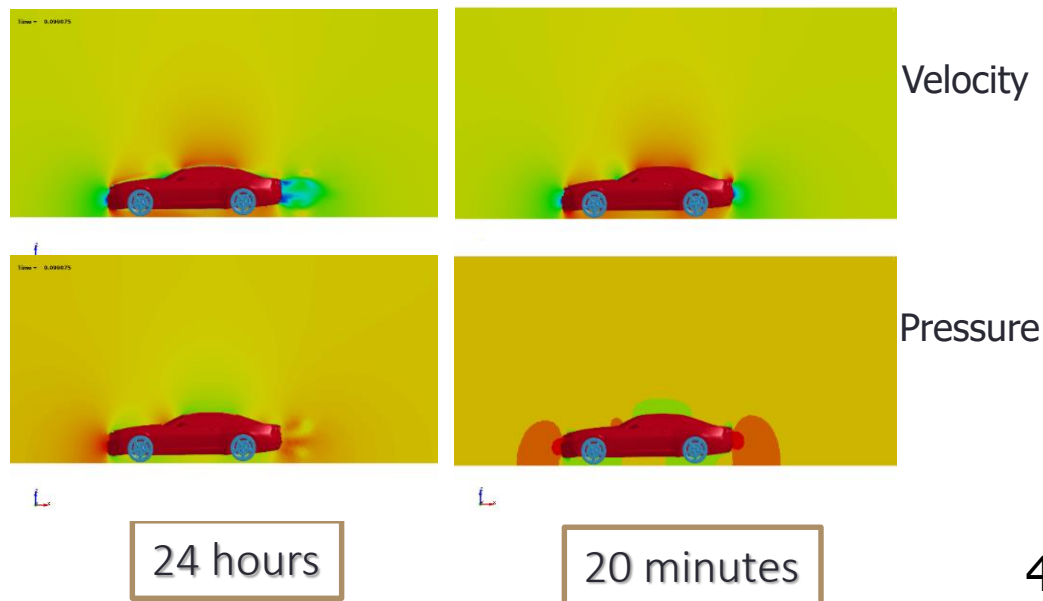
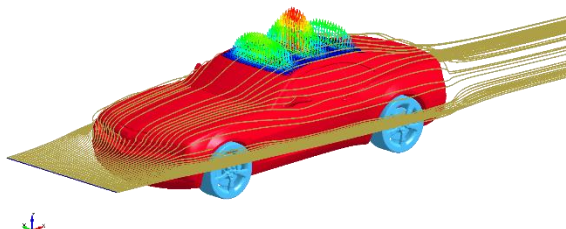
- Conjugate heat transfer for die casting

Navier Stokes

Potential Flow

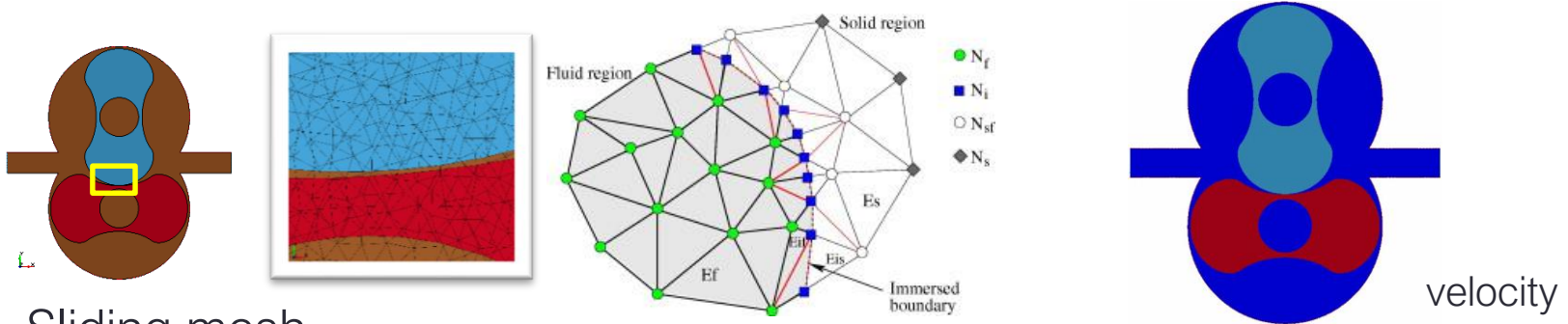


- FSI

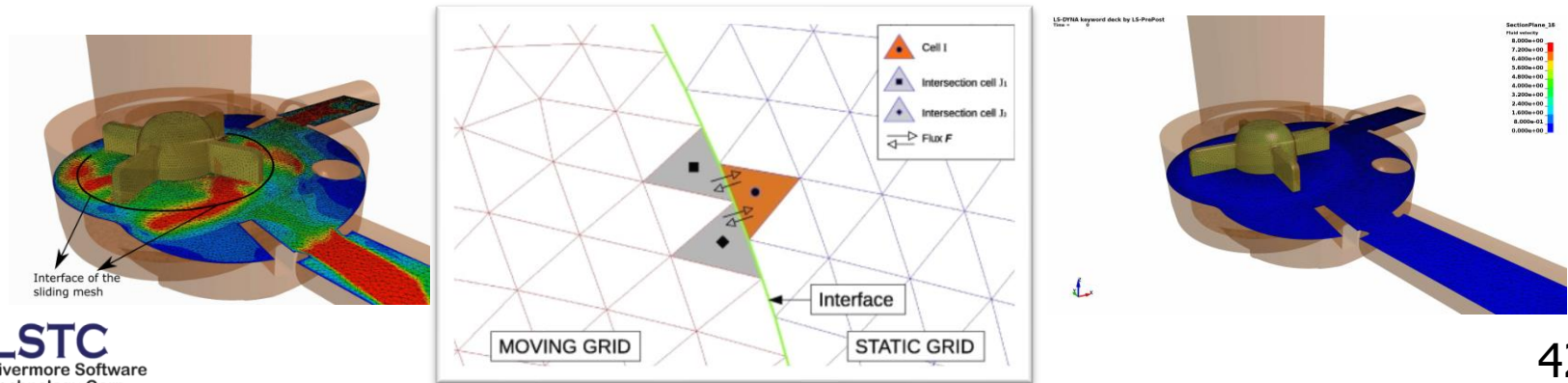


Immersed Interface & sliding mesh

- Immersed interfaces
 - simplifies the pre-processing of complex geometries.
 - provide sharp interfaces and allow structural contact.

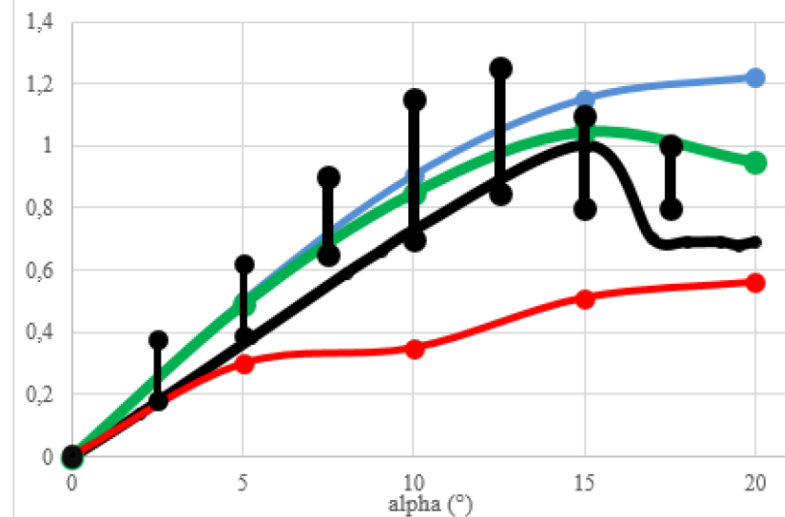
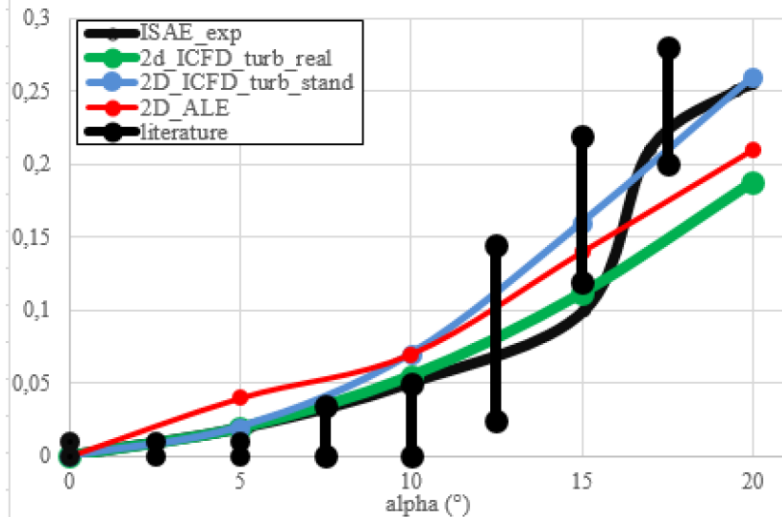
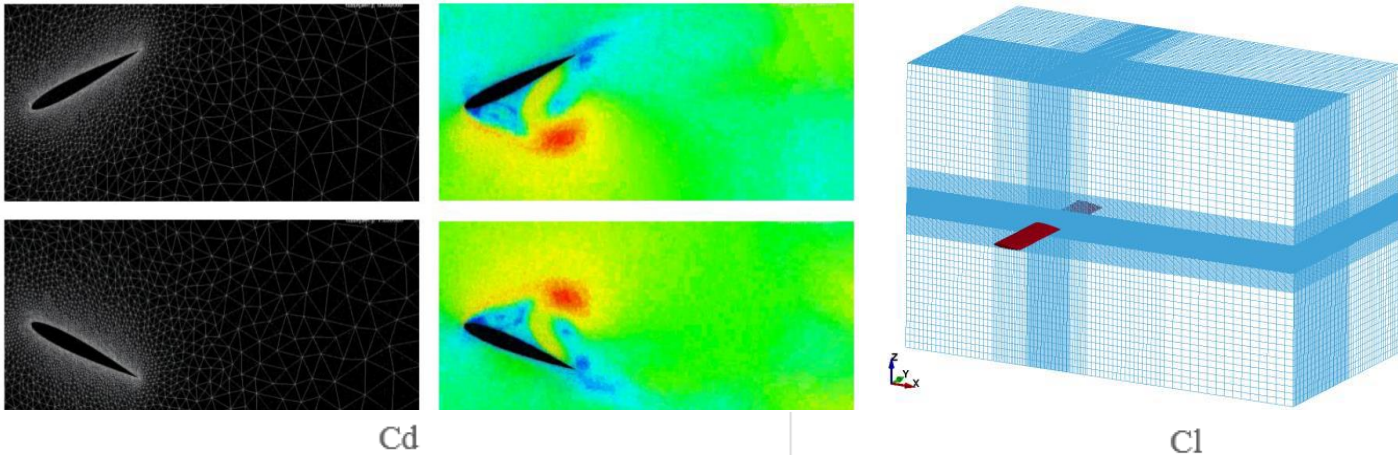


- Sliding mesh
 - for the simulation of transient rotating mechanisms without re-meshing.
 - the domain is split into at least two volume meshes. One mesh will have the rotating components and the other the rest of the domain
 - prevents excessive re-meshing in problems that involve rotating parts



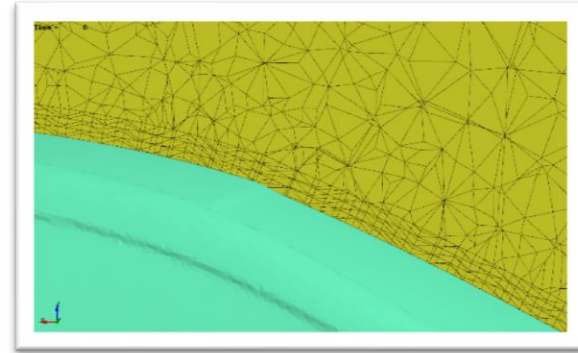
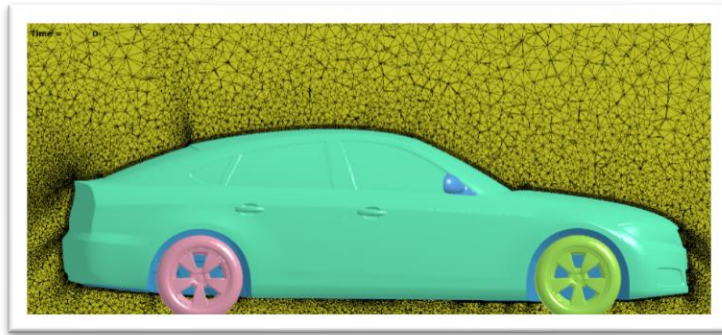
Compare ALE and ICFD based on airfoil simulation

- Based on NACA0012

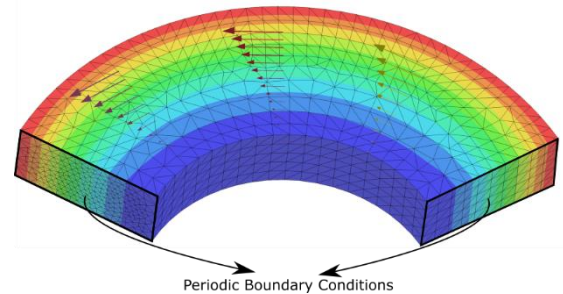
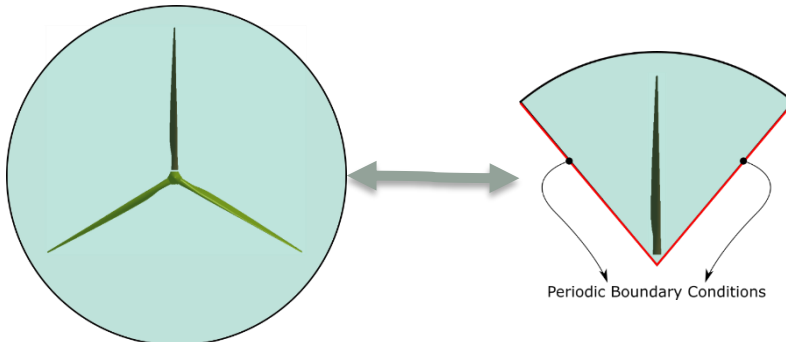


Boundary Layer and periodic boundary condition

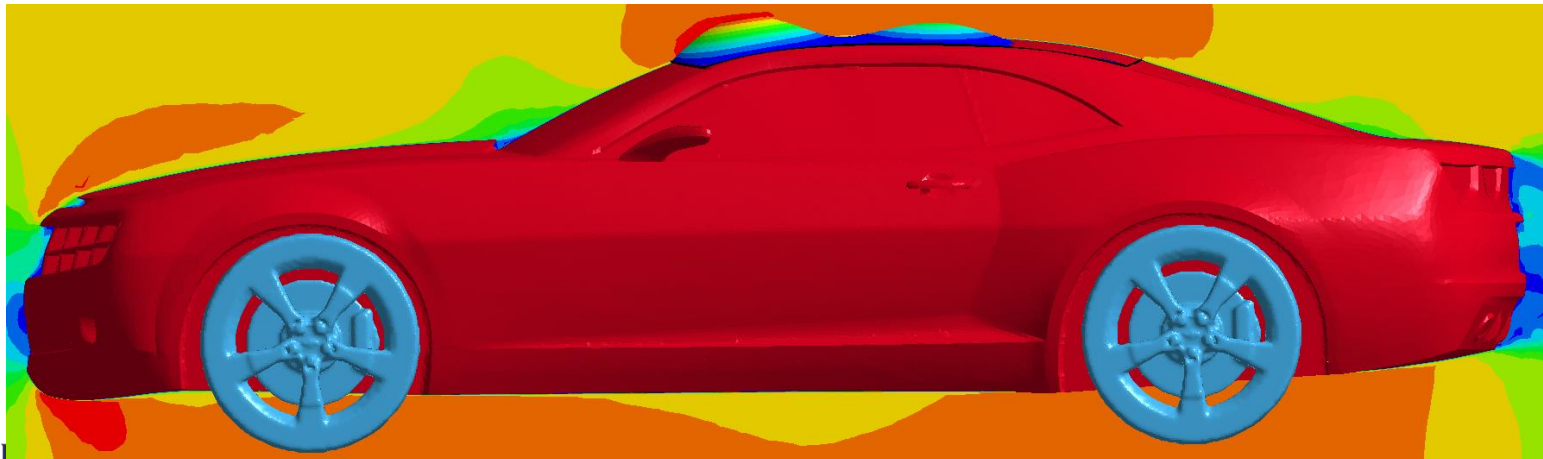
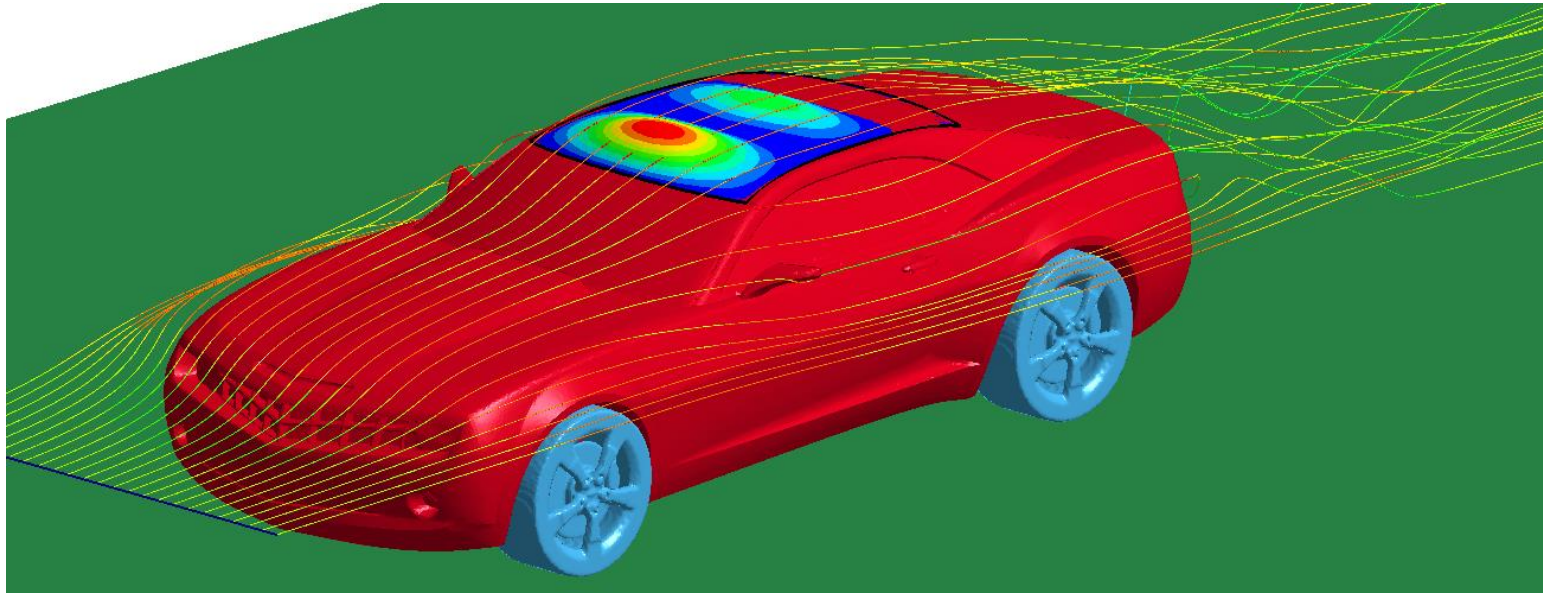
- Boundary layer and new RANS turbulence model
 - improvements in speed and quality of boundary layer mesh generation
 - Most commonly encountered RANS Turbulence models are available



- Periodic boundary condition
 - allow a domain reduction of the areas with a repeating fluid pattern. It is widely used in the simulation of turbomachinery.



Coupling IGA with ICFD

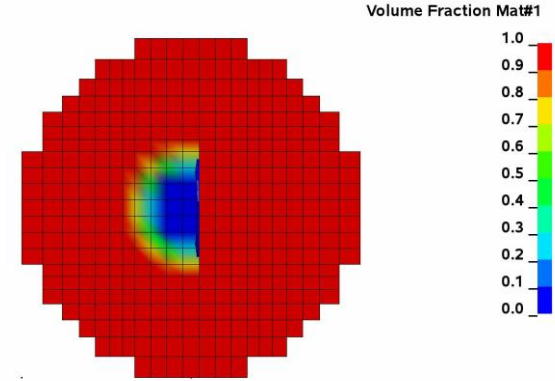


ALE

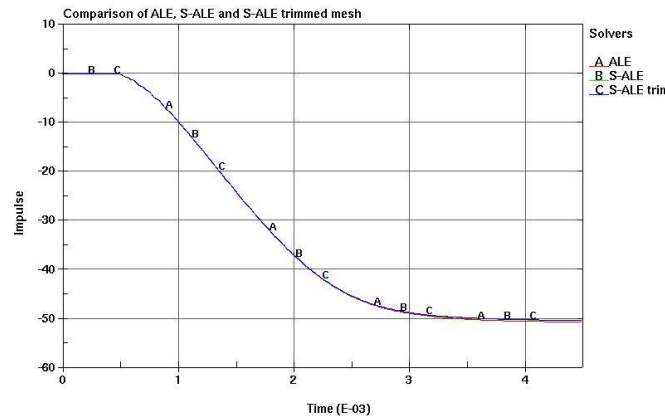
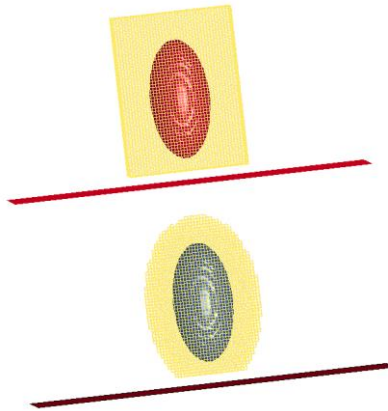
S-ALE: Mesh Trimming

- ALE_STRUCTURED_MESH_T
RIM trims off unnecessary
elements.

Time = 0
Contours of Volume Fraction Mat#1
max IP value
min=0, at elem# 203728
max=1, at elem# 200156



<http://ftp.lstc.com/anonymous/outgoing/hao/sale/models/meshtrim/saletrim.tar>



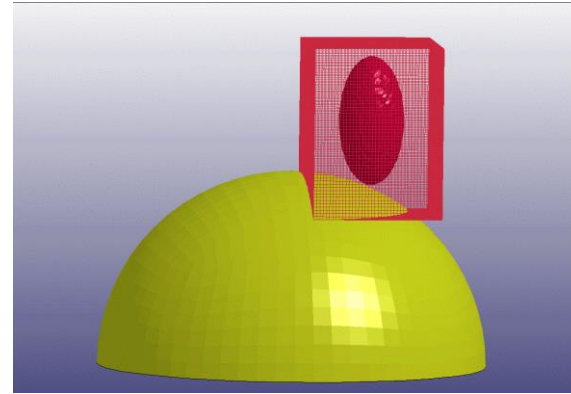
Results consistency

method	# of ele	time
ALE	84800	1.0
S-ALE	84800	0.6
S-ALE_TRIM	43219	0.35

CPU time / MPP 4 cores

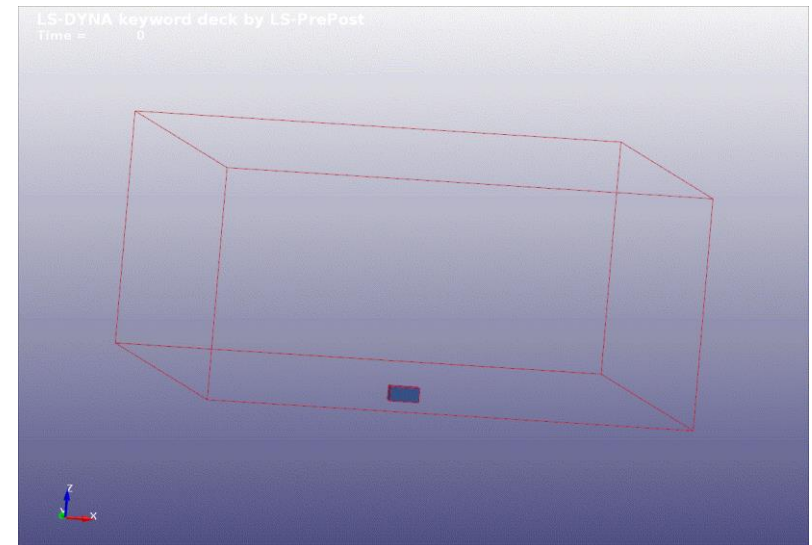
S-ALE: FOLLOW_GC & mesh merging

- New option of FOLLOW_GC of ALE_STRUCTURED_MESH_MOTION move the ALE mesh with the gravity center of certain AMMG groups; and expand/contract with those fluids.



http://ftp.lstc.com/anonymous/outgoing/hao/sale/models/meshmotion/birdstrike/bird_sale.tar

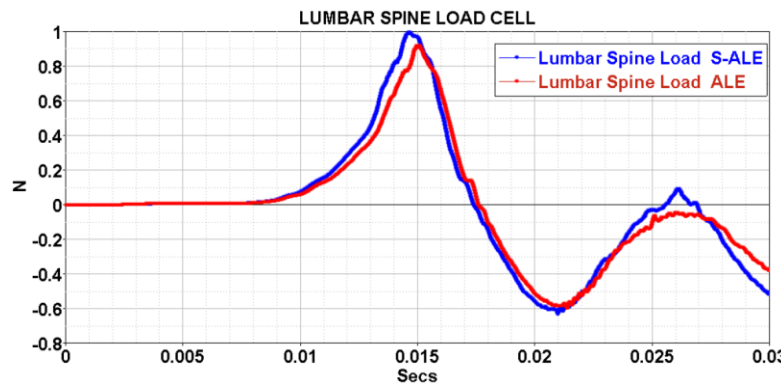
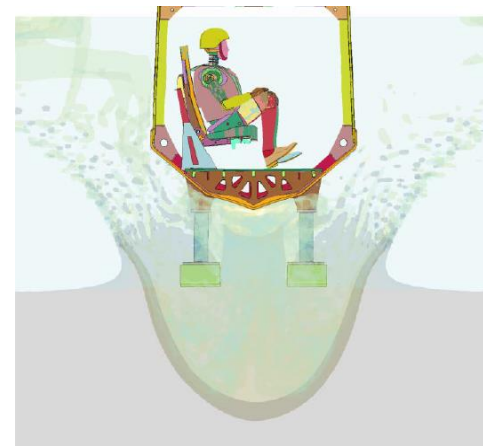
- Multiple ALE_STRUCTURED_MESH cards. Can share the same PID
 - A finer mesh for HE and solid can share the same PID with the coarser air mesh separately created by other ALE_STRUCTURED_MESH card



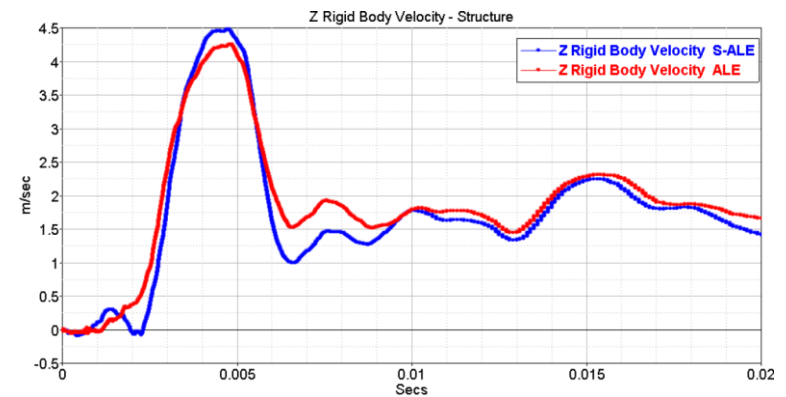
two meshes setup reduced mesh usage from 6 million to 4 million.

S-ALE vs. ALE for blast simulation

- Save 28% of CPU with comparable results



Slider response



structure response

Phase Change EOS for ALE FSI

- In order to simulate fast transient phenomena such as Water Hammers or UNDEX, one must take into consideration phase change.
- Homogeneous Equilibrium Model (HEM) is one of the “one-fluid models” where only the average flow is considered by solving a unique set of governing equations and it can be based on a pure phase model.

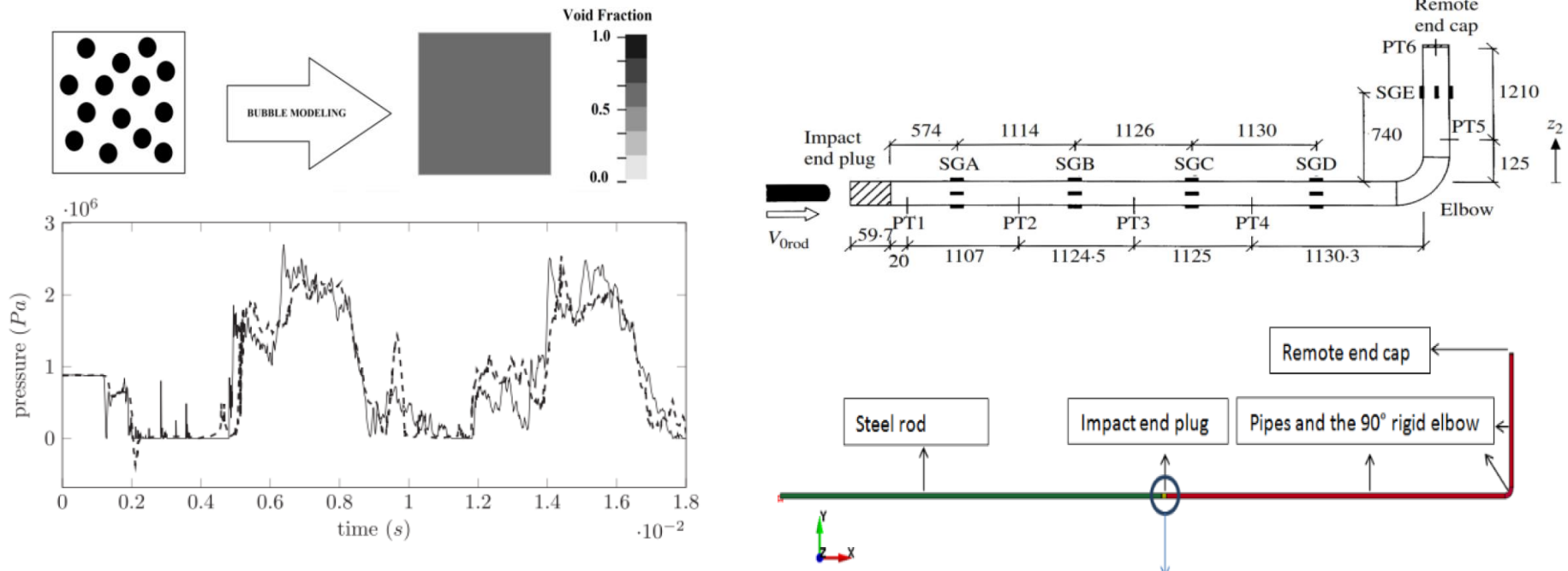
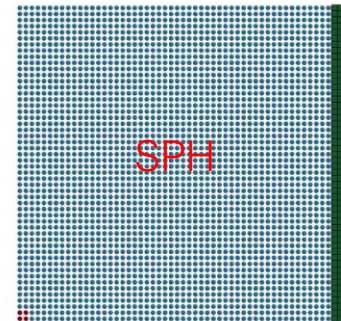
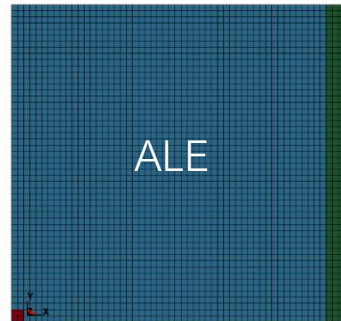
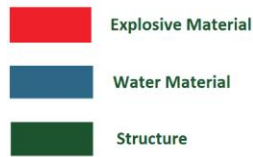


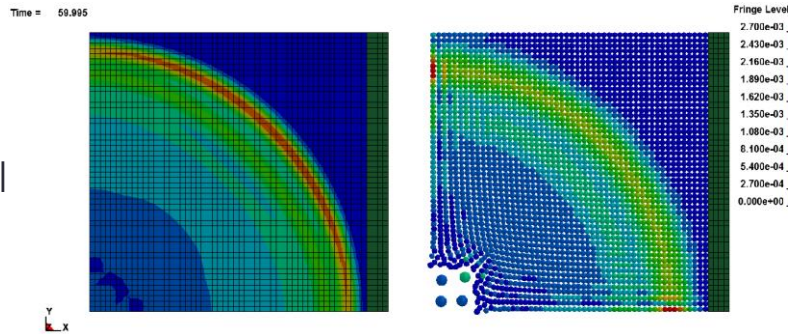
Figure 4: Absolute pressure at sensor PT6: Experimental results Tijsseling et al., [8], (- -), numerical results with elastic pipes (—).

SPH

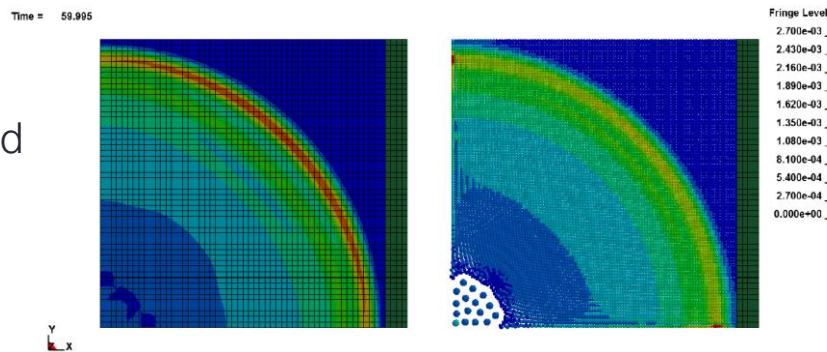
Comparing SPH & ALE for UNDEX



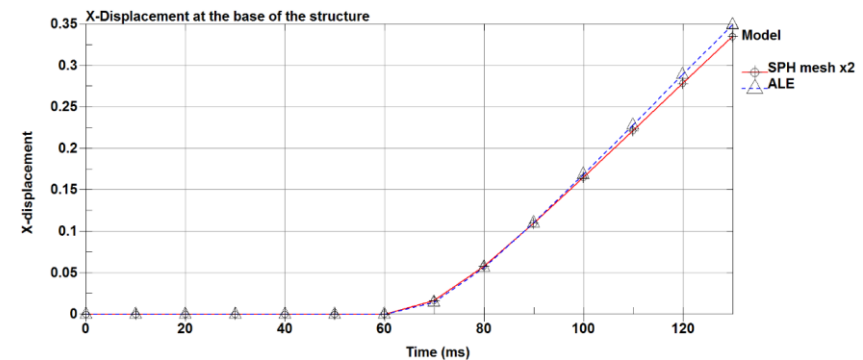
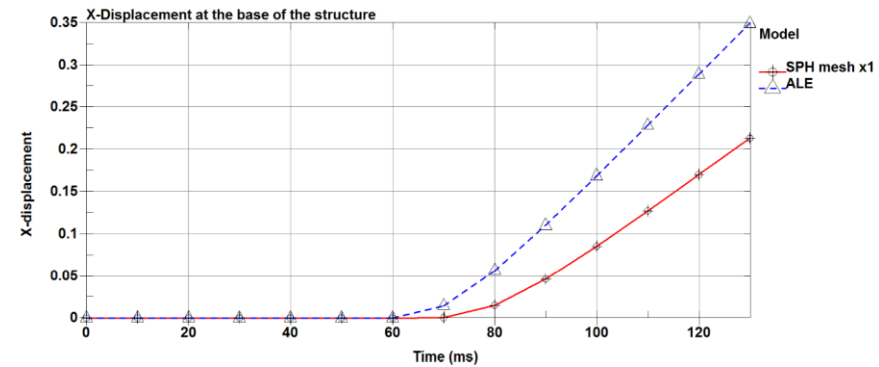
Original
SPH



Refined
SPH



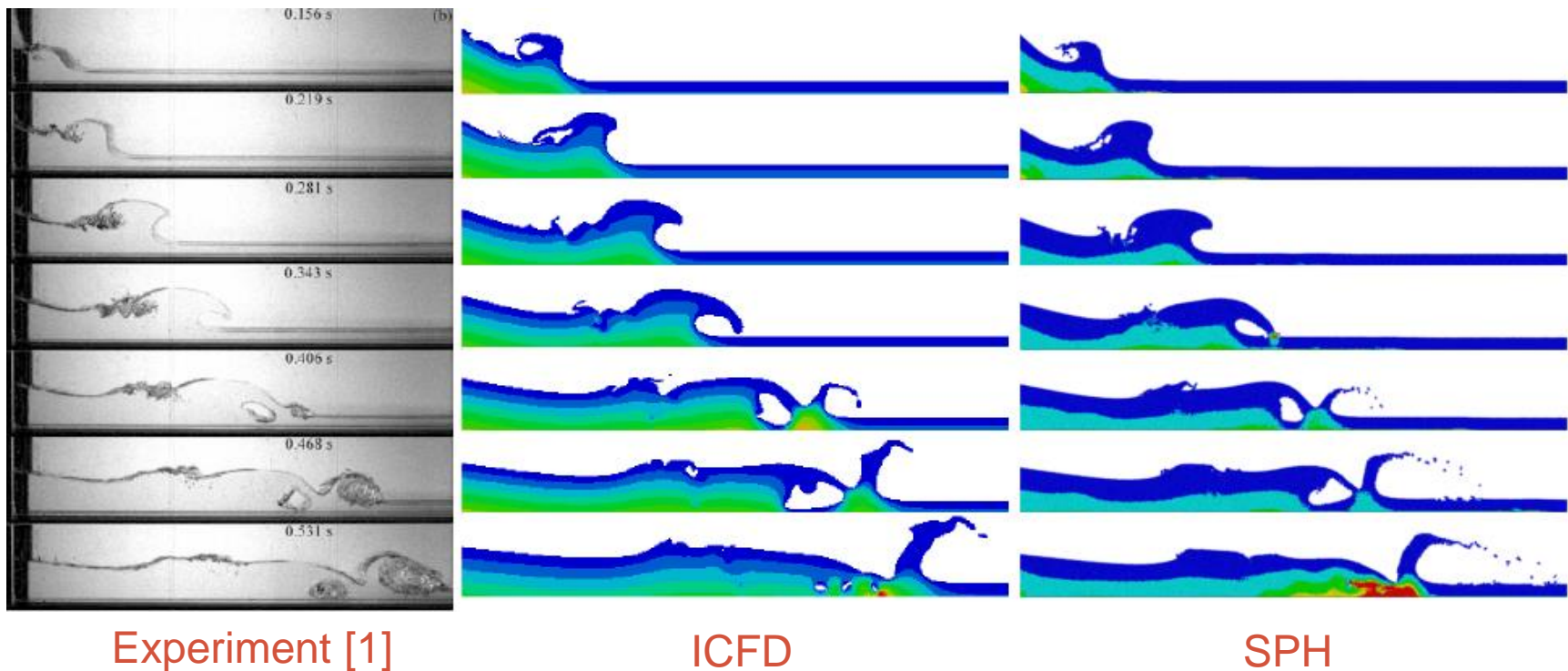
Pressure contour



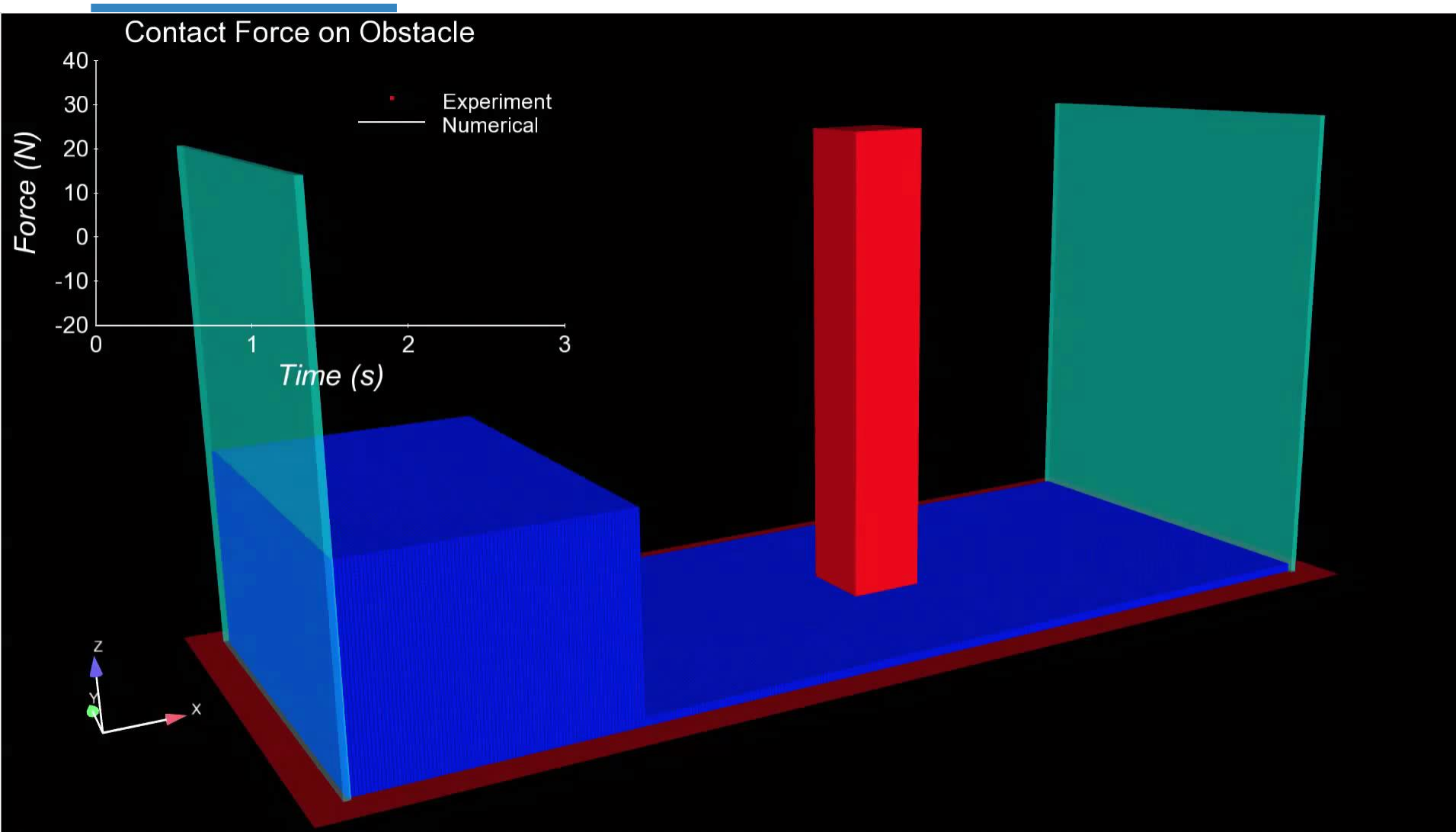
SPH: Murnaghan Equation of State, IFORM=15/16

- Model incompressible fluid with SPH elements
- Weakly compressible formulation to numerically reduce the sound speed, and consequently increase the time step size

Validation: 2D dambreak, free surface flow

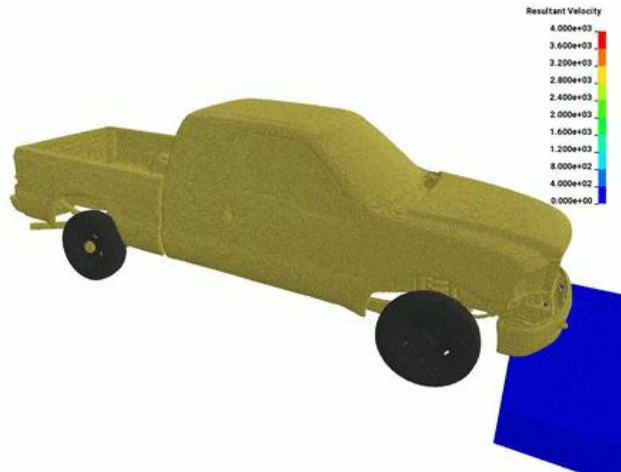


SPH: 3D Validation of Murnaghan Equation of State

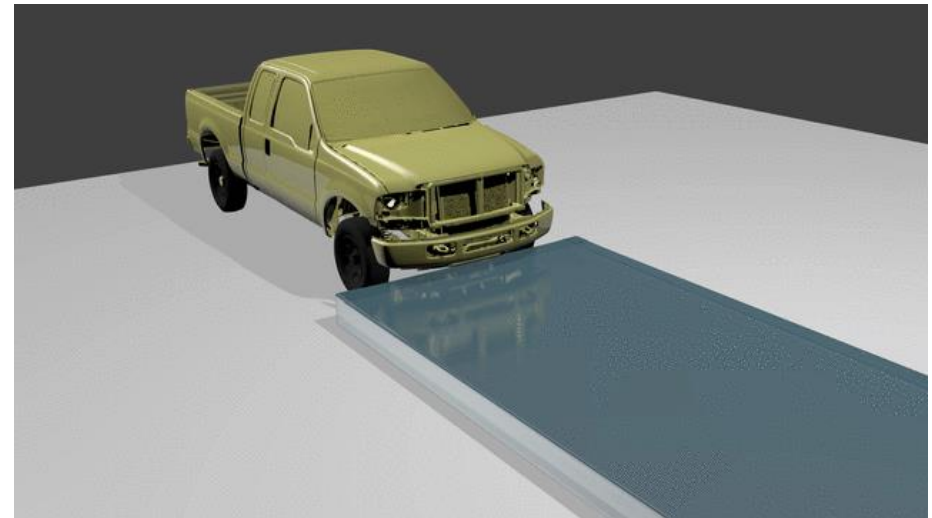


Implicit SPH

- Implicit, incompressible SPH formulation allows larger timestep size
- Tailored for wading-type problems
- Example with 9.1 million particles:



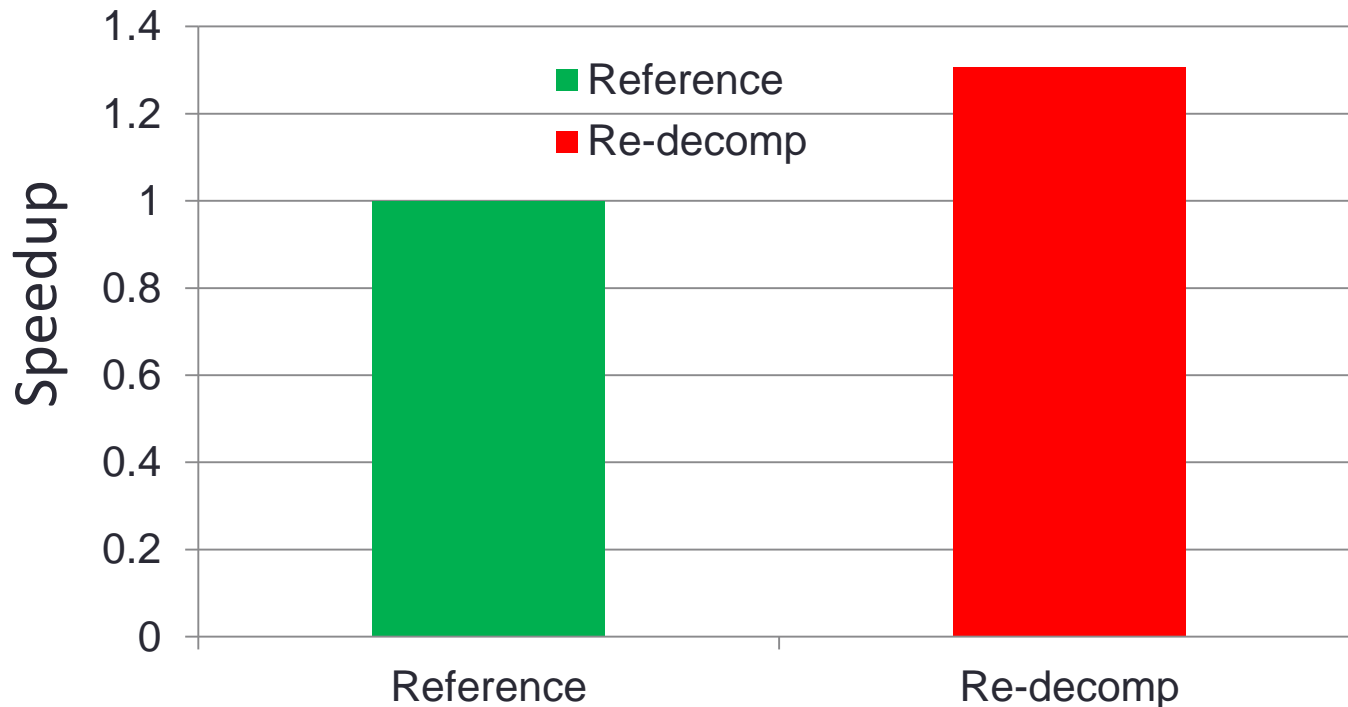
*Implicit SPH
Color-coded by velocity*



Blender rendering

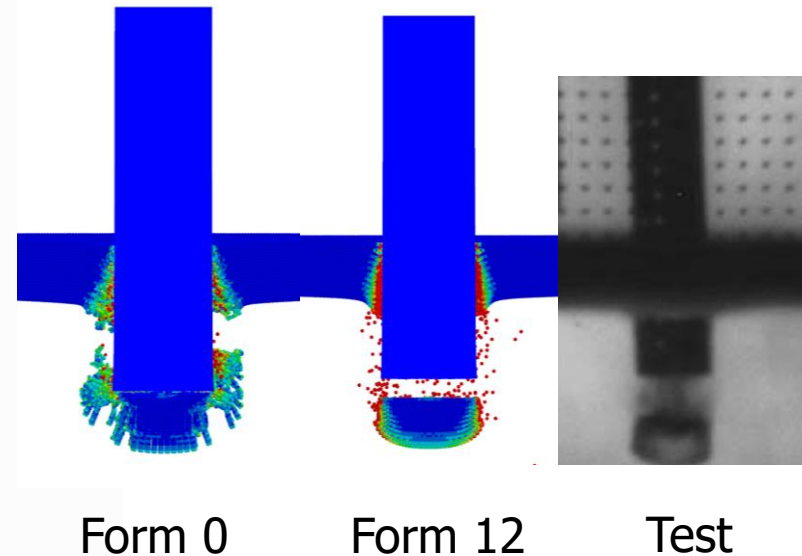
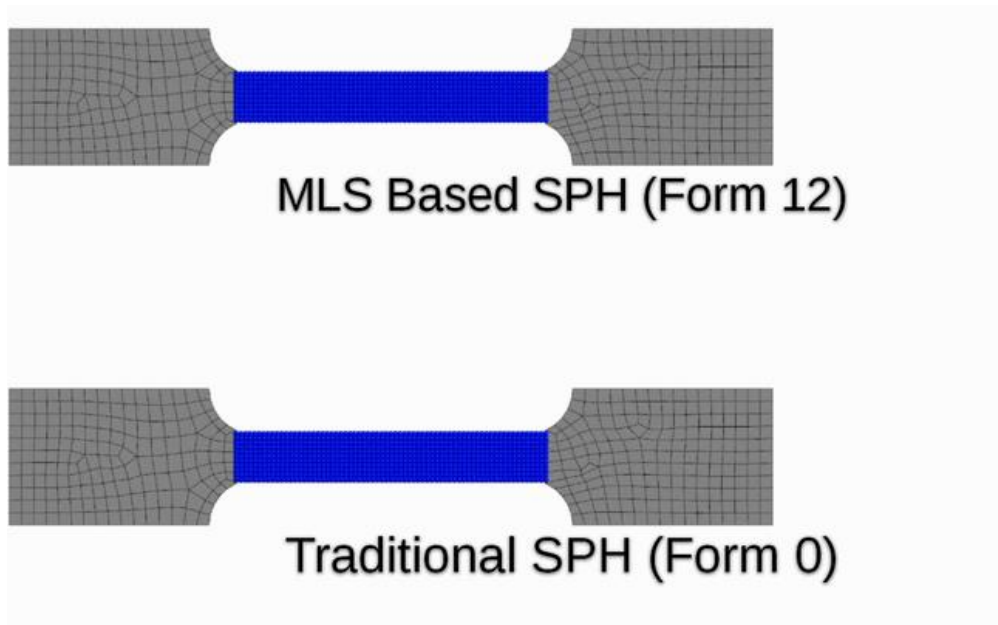
Dynamically Rebalanced SPH

- Re-decomposed the model several times during simulation using a full deck restart
- 30% of cpu saving is observe in a typical bird strike simulation



MLS-based SPH

- A formulation based on moving least-squares (FORM = 12) is implemented to improve the major drawbacks associated with SPH: tensile instability and essential boundary condition enforcement. Moving Least Square formulaton.

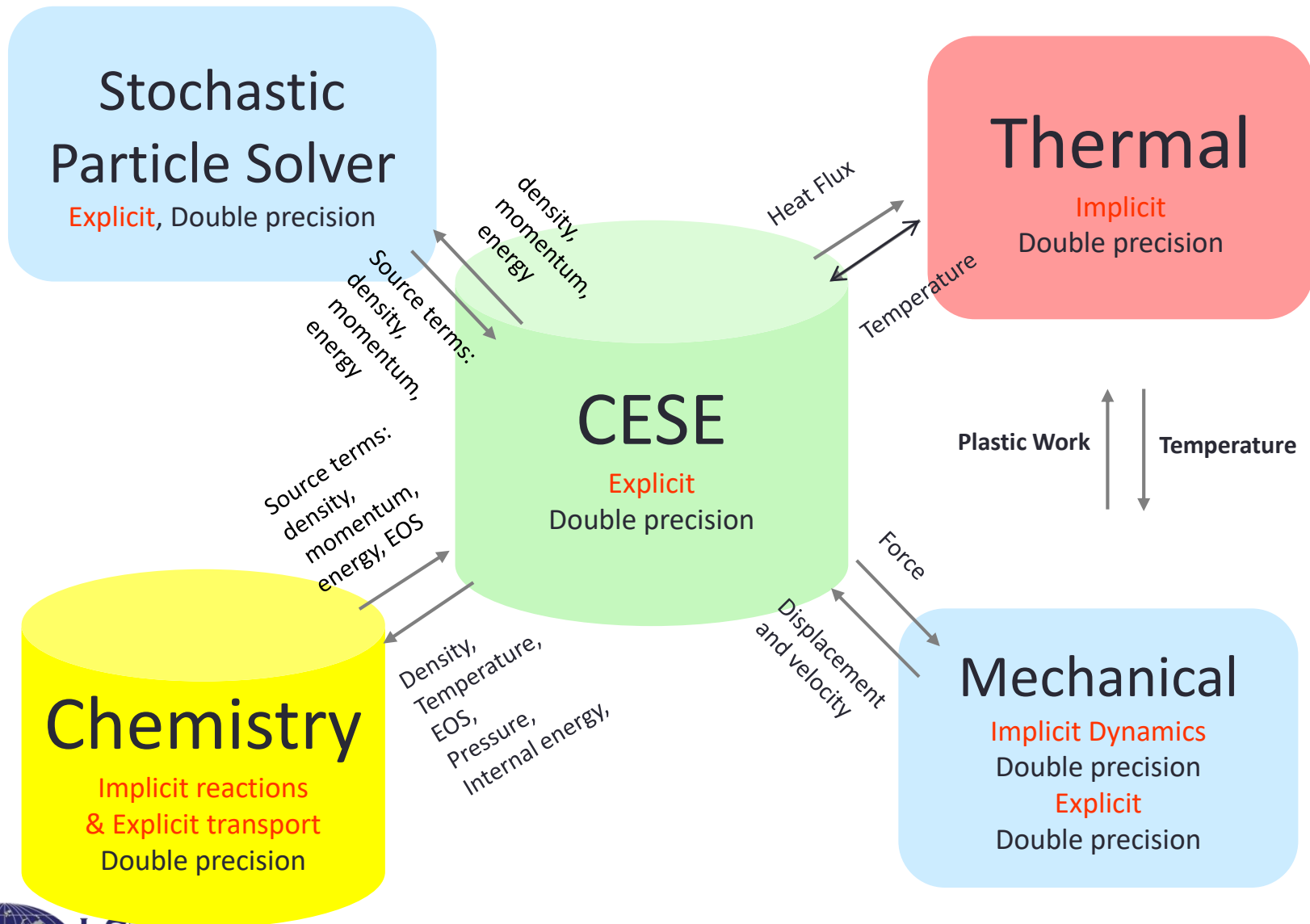


T Borvik et al. "Perforation of 12 mm thick steel plates by 20 mm diameter projectiles with flat, hemispherical and conical noses: Part I: Experimental study". *International Journal of Impact Engineering* 27.1 (2002).

CESE and Chemistry Solvers

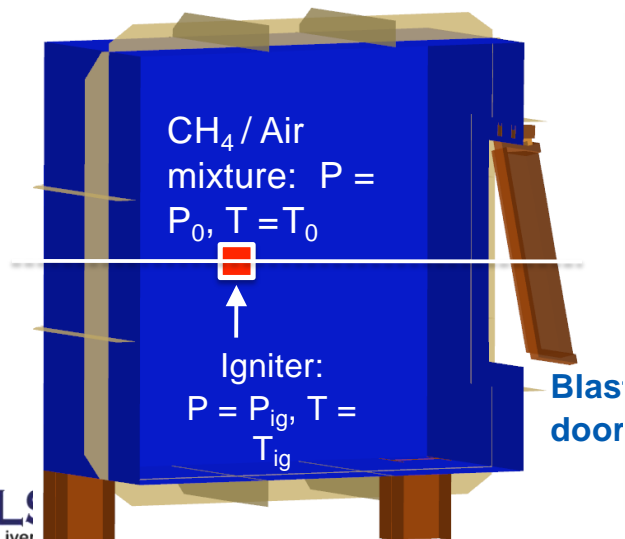
Zeng-chan Zhang, Kyoung-Su Im, and Grant Cook, Jr.

CESE coupling with other LS-DYNA solvers

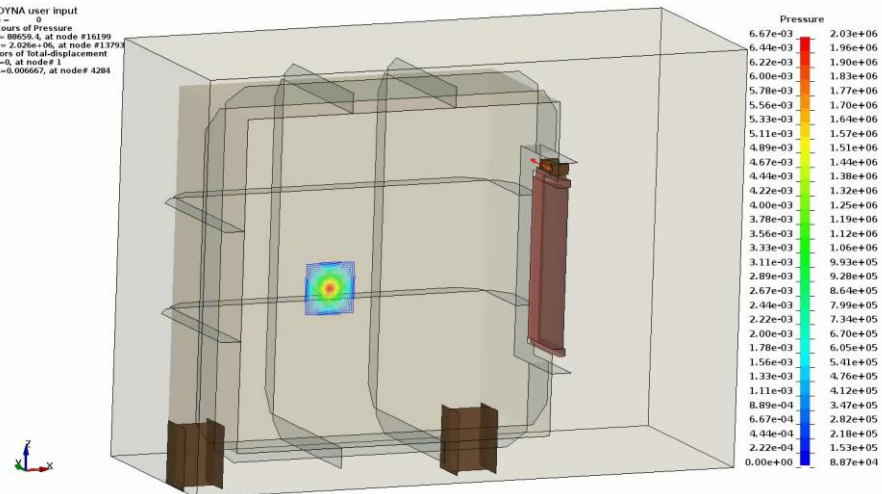


CESE for blast relief valve

- The purpose of the blast relief wall is to vent the combustion gases and pressure resulting from a deflagration of an enclosure in offshore plant. Gas mixture consists of air and methane (CH₄).



LS-DYNA user input
Time = 0
Contours of Pressure
min = 88659.4, at node #16199
max = 2.026e+06, at node #13794
Vectors of total-displacement
min=0, at node# 1
max=0.006667, at node# 4284



Meshless & particle methods

SPH

J. Xu

ALE

H. Chen

DEM

H. Tang, B. Zhang

SPG

Y. Wu, C.T. Wu

Peridynamics

W. Hu, B. Ren, C.T. Wu

XFEM

Y. Guo, C.T. Wu

Meshfree & Particle Methods in LS-DYNA

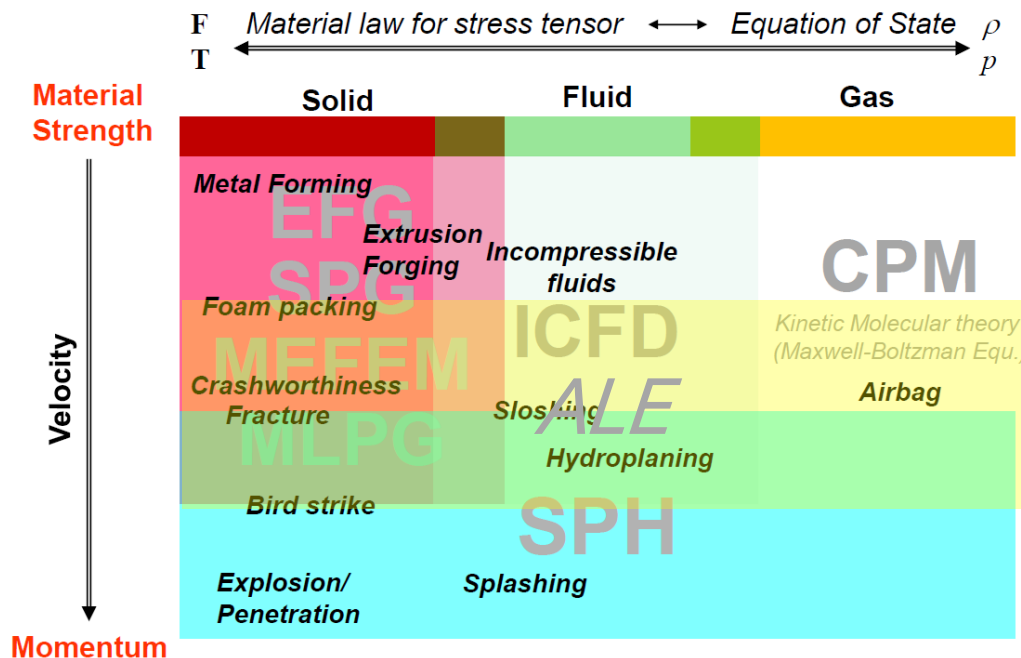
Discrete

Explicit

- DEM (Discrete Element Method)
- CPM (Particle Gas)
- PARTICLE_BLAST

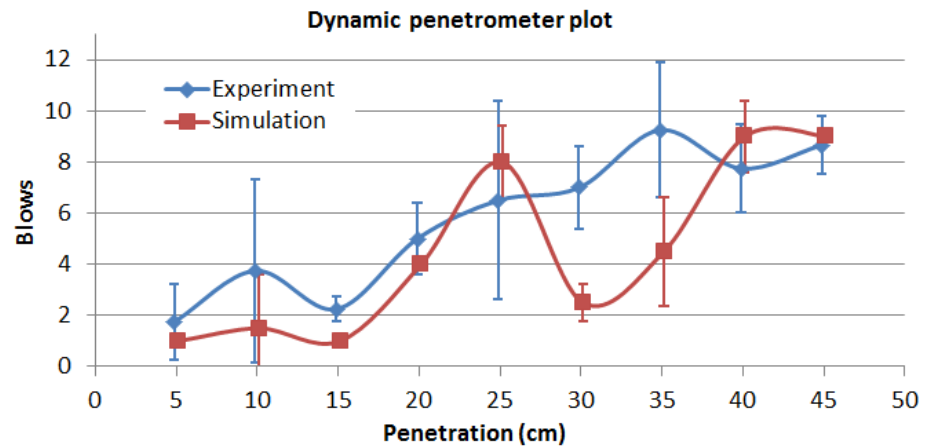
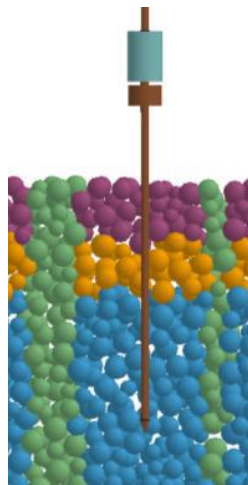
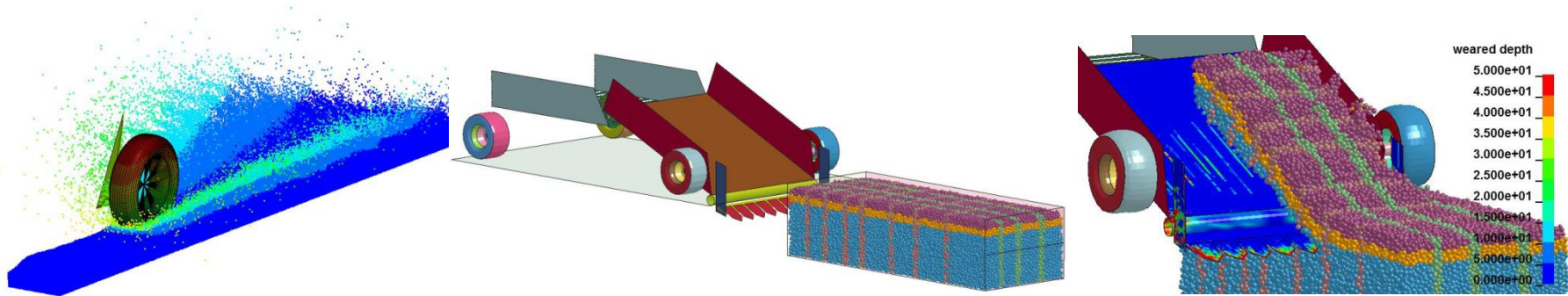
Continuum

- Explicit Meshfree Collocation
 - SPH
- Explicit Meshfree Galerkin
 - EFG, SOLID41&42, SHELL41~44
 - XFEM: SHELL52&54
 - MEFEM for nearly incompressible material, SOLID43
 - SPG (Smooth Particle Galerkin), SOLID47 for ductile failure
 - Peridynamics (Discontinuous Galerkin) for brittle fracture, SOLID48&MAT_ELASTIC_PERI
- Implicit Meshfree Galerkin
 - EFG, SOLID41&42, SHELL41~44
 - MEFEM, SOLID43



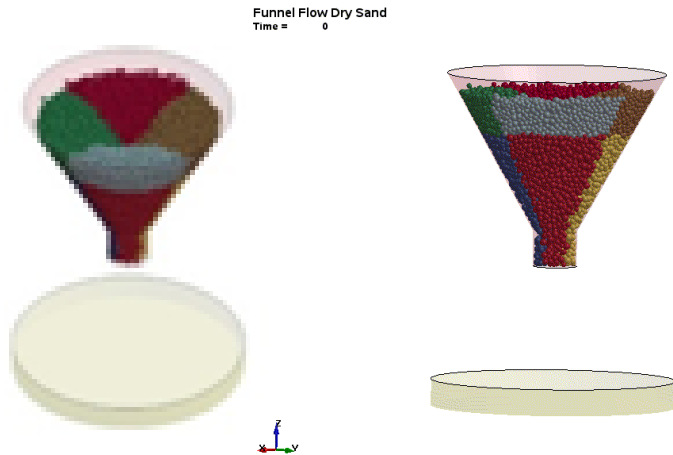
DEM

- for granular materials that consist of discrete particles like liquids and solutions, cereal, sand, toner,...



DEM: DE-DE contact improvement

- MPP scalability could deteriorate due to load imbalance when particles undergo large motion



- re-decompose for every N time steps



- Performance improvement

LS-DYNA keyword deck by LS-PrePost
Time = 0

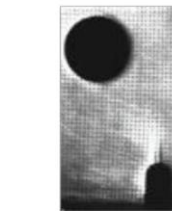
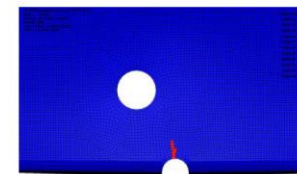
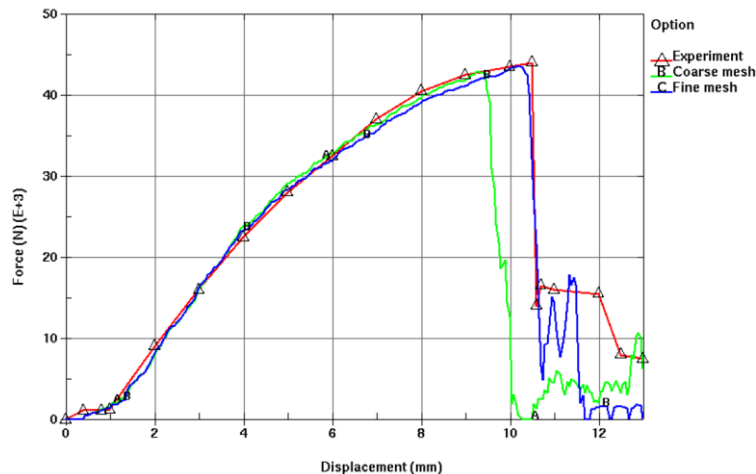
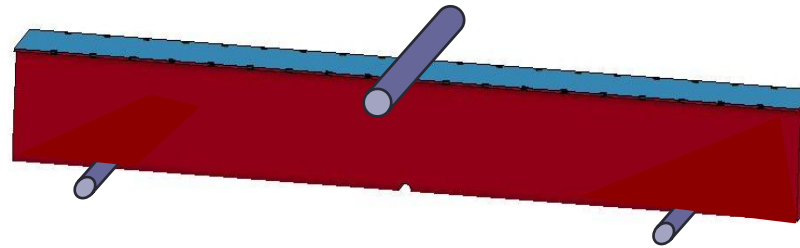


SPEEDUP

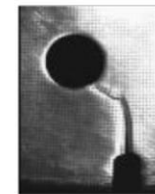
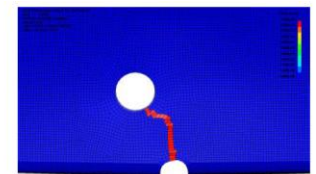


XFEM

- Most suitable for ductile materials in shell formulation, especially for pre-cracks
- A non-local algorithm is developed to minimize the mesh-size/orientation problems



(a) Initial crack



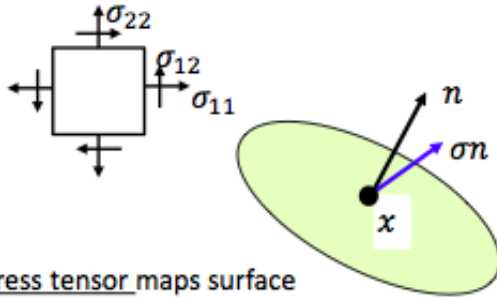
(b) Intermediate crack

Peridynamics Method

- Extension of classical pdf-based equation.

Standard theory

Stress tensor field
(assumes continuity of forces)



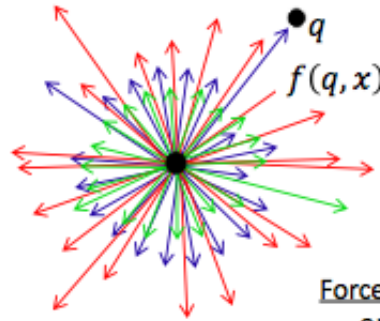
Stress tensor maps surface normal vectors onto surface forces

$$\rho \ddot{u}(x, t) = \nabla \cdot \sigma(x, t) + b(x, t)$$

Differentiation of surface forces

Peridynamics

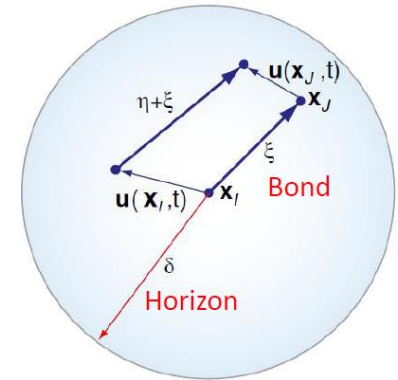
Bond forces between neighboring points
(allowing discontinuity)



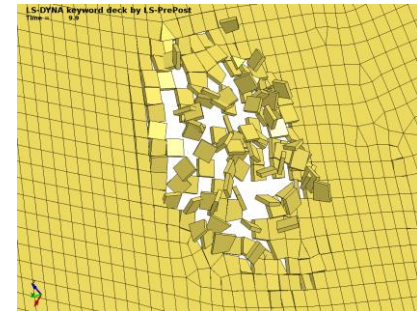
Force state maps bonds onto bond forces

$$\rho \ddot{u}(x, t) = \int_{H_x} f(q, x) dV_q + b(x, t)$$

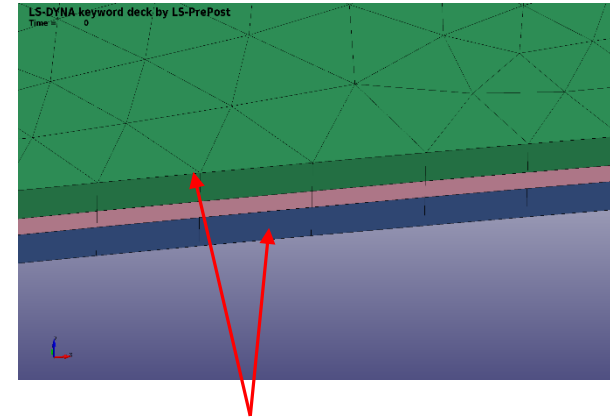
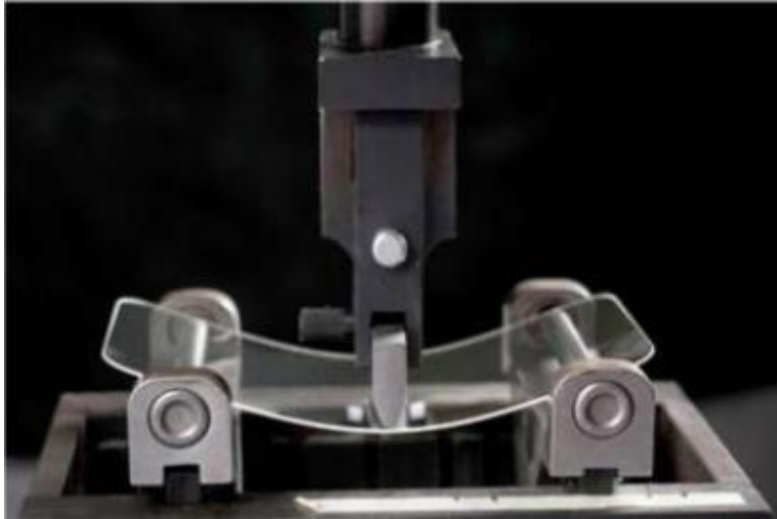
Summation over bond forces



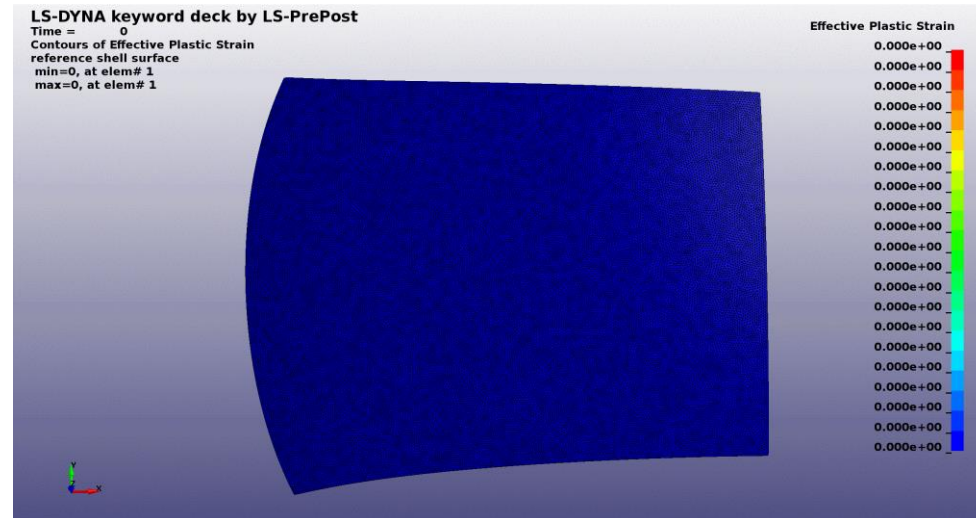
- Most suitable for brittle materials in 3D solid formulation.
- Modified version formulated in Discontinuous Galerkin FEM
- Failure criteria is based on fracture energy released rate



Peridynamics for windshield 3-point bending analysis



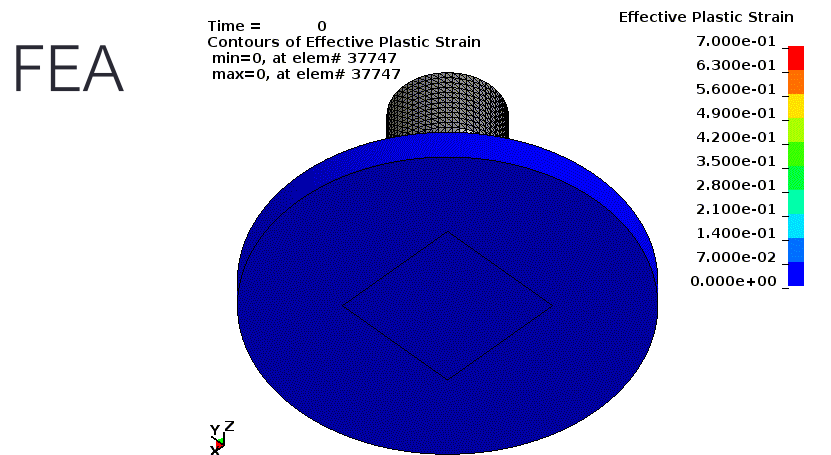
Glass layers, MAT_ELASTIC_PERI



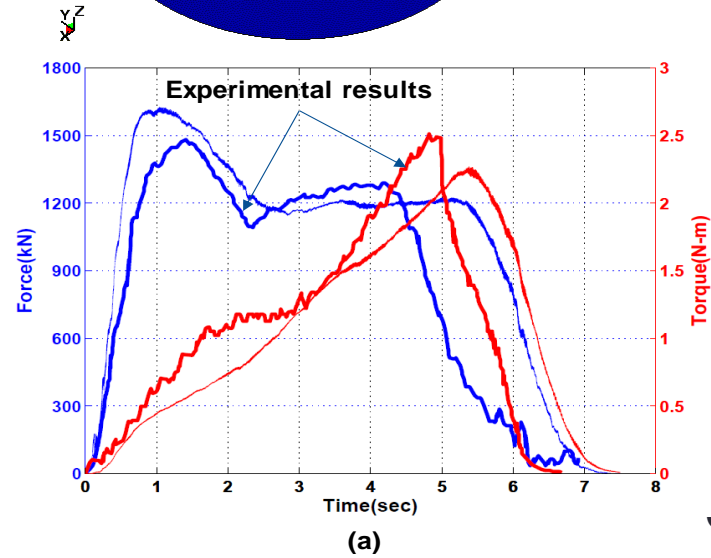
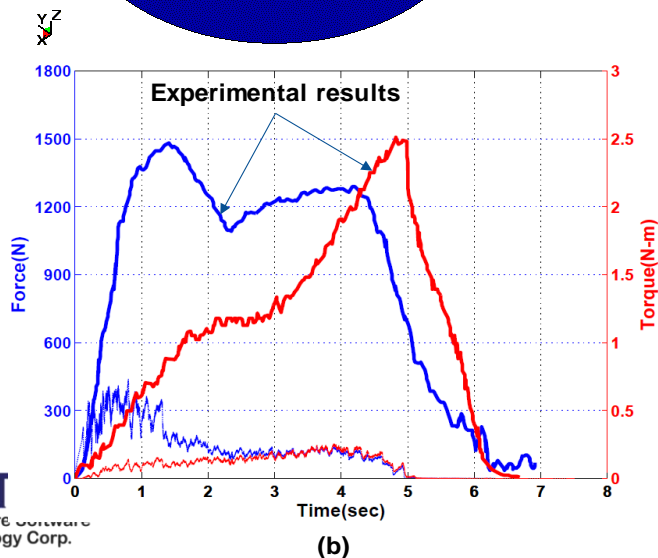
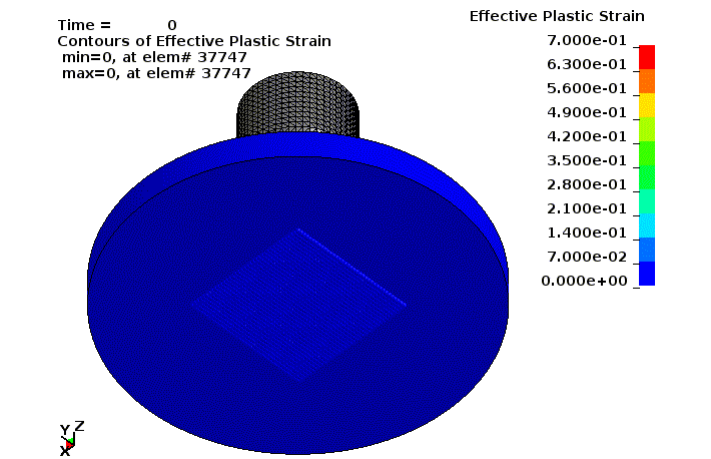
Maximum Force (N)		Displacement (mm)	
Exp.	Num.	Exp.	Num.
2841	2860	24.6	26.0

SPG

- Particle integration, able to handle severe deformation
- Most suitable for ductile materials in 3D solid formulation.
- Applications include machining, joining, cutting, riveting & drilling



SPG



Summary

- LSTC is working to be the leader in cost effective large scale numerical simulations
- LSTC is providing dummy, barrier, and head form models to reduce customer costs.
- LS-PrePost, LS-Opt, and LS-TaSC are continuously improving and gaining more usage within the LS-DYNA user community
- LSTC is actively working on seamless multistage simulations in automotive crashworthiness, manufacturing, and aerospace
- The scalable implicit solver is quickly gaining market acceptance for linear/nonlinear implicit calculations and simulations
- Robustness, speed, accuracy, and scalability have rapidly improved

Future

- New features and algorithms will be continuously implemented to handle new challenges and applications
 - Electromagnetics,
 - Acoustics,
 - Compressible and incompressible fluids
 - Isogeometric shell, solid elements and NURB contact algorithms
 - Discrete element methodology for modeling granular materials, failure, etc.
 - Peridynamics combined with EFG and DES
 - Composite material manufacturing
 - Modeling battery response in crashworthiness simulations
 - Sparse solver developments for scalability to huge # of cores, >10K

12th LS-DYNA European Conference

14 - 16 May 2019, Koblenz, Germany

